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January 23, 2020

Ms. Tania Taff
Air Management Engineer – Division of Environmental Management
Wisconsin Department of Natural Resources
2984 Shawano Ave
Green Bay, WI 54313-6727

RE: Testing for emissions of mercury from I08 without use of granulated activated carbon

Dear Ms. Taff:

The purpose of this letter is to submit and discuss results for emissions testing that Green Bay Metropolitan Sewerage District (GBMSD) has opted to conduct on Process I08, the fluid bed incinerator.

### Background

In 2018, GBMSD began operation of a new fluid bed incinerator (FBI) that is subject to 40 CFR 60, Subpart LLLL, Standards of Performance for New Sewage Sludge Incineration Units, which include limits for mercury emissions. GBMSD installed a granulated activated carbon (GAC) unit to control mercury emissions, if needed, to meet the new limits. Compliance emissions testing in October 2018 and May 2019 demonstrated that mercury emissions have been within the limits while operating the GAC.

A malfunction that occurred on November 7, 2019, described in a written report to the United States Environmental Protection Agency (US EPA) dated December 31, 2019, left the GAC inoperable. GBMSD implemented numerous alternative options for managing sludge, but after several weeks, determined that the ability to treat wastewater effectively would be compromised without incinerating some sewage sludge. As such, limited incineration of sewage sludge without the GAC began on November 21, 2019.

GBMSD I08 Emission Test without GAC (Mercury) Page 2 of 4 January 23, 2020

To measure the mercury emission rate and evaluate the potential impacts of operating without the GAC, GBMSD conduct an emission test on December 12, 2019. All other emission control systems, (the combustion chamber temperature, a wet electrostatic precipitator, and scrubber) operate in accordance with their respective allowable operating parameters whenever the FBI is operated, including during the emission test. The enclosed report contains the results from that testing, which was conducted by Advanced Industrial Resources, Inc. Results show that the allowable mercury concentration exceeded the Subpart LLLL limit for new fluid bed incinerators while incinerating sewage sludge without operating the GAC.

While operating the FBI without the GAC might exceed the allowable mercury concentration, it does not pose a significant risk to the public. An air dispersion modeling evaluation was conducted by using the measured mercury emission rate without the GAC and comparing the results with health-based standards. The evaluation demonstrates that the impacts from the emission rate are well within state health-based standards. This evaluation is discussed in detail below.

### Discussion

GBMSD conducted an emission test on December 12, 2019 to determine the mercury emission rate from the FBI without the GAC operating. The sludge feed rate during the test averaged 1.81 dry tons per hour, which is 85% of the 51 dry tons per 24-hour day capacity.

The measured mercury emission concentration from the December 12, 2019 test was 0.0220 milligrams per cubic meter (mg/m³) corrected to 7% oxygen. While this emission concentration exceeds the Subpart LLLL emission limit, it meets several other standards, including the Subpart LLLL limit for new multiple hearth sewage sludge incinerators, as well as existing fluid bed and multiple hearth sewage sludge incinerators (see 40 CFR 60 Subpart MMMM). The measured mercury emission rate was 0.000646 pounds per hour (lb/hr), which meets the National Emission Standard for Mercury (see 40 CFR 61 Subpart E). This emission rate also meets Wisconsin's air toxics emissions standards for mercury (see Wis. Admin. Code§ NR 445, Table A). Table 1 compares the measured concentration and emission rate without the GAC in operation with each of these federal and state standards.

GBMSD I08 Emission Test without GAC (Mercury) Page 3 of 4 January 23, 2020

Table 1 Comparison of Mercury Emission Rate without GAC with Federal and State Standards

Table 1 Comparison of Mercury Emission Rate Willout CAO Will 1 ederar and Otate Guman					
Regulation	Numeric Standard	Equivalent Hourly Standard	GBMSD FBI without GAC <sup>1</sup>	Meets Standard, Percent	
Federal Standards					
Subpart LLLL	0.0010 mg/m <sup>3</sup>		0.0220 mg/m <sup>3</sup>	Exceeds	
New Fluid Bed Incinerator	@ 7% O <sub>2</sub>		@ 7% O <sub>2</sub>	Standard	
Subpart LLLL	0.15 mg/m <sup>3</sup>		0.0220 mg/m <sup>3</sup>	15 %	
New Multiple Hearth Incinerator	(@ 7% O₂		@ 7% O <sub>2</sub>	10 70	
Subpart MMMM	0.037 mg/m <sup>3</sup>		0.0220 mg/m <sup>3</sup>	59 %	
Existing Fluid Bed Incinerator	@ 7% O <sub>2</sub>		@ 7% O <sub>2</sub>	J9 70	
Subpart MMMM	0.28 mg/m <sup>3</sup>		0.0220 mg/m <sup>3</sup>		
Existing Multiple Hearth	@ 7% O <sub>2</sub>		@ 7% O <sub>2</sub>	8 %	
Incinerator	€ 7 7 ° 2		G		
40 CFR 61 Subpart E	7.1 lb/24-hr	0.30 lb/hr	0.000646 lb/hr	0.2 %	
Sludge Incineration Plants					
Wisconsin State Standards					
NR 446.20(2)	7.1 lb/24-hr	0.30 lb/hr	0.000646 lb/hr	0.2 %	
Sludge Incineration Plants					
NR 445 Table A				0.004	
Mercury, Inorganic	1,838 lb/yr	0.21 lb/hr	0.000646 lb/hr	0.3 %	
Stack Ht > 75 ft				***************************************	
NR 445 Table A					
Mercury, Inorganic	0.0405 lb/hr		0.000646 lb/hr	2 %	
Stack Ht > 75 ft					

To estimate potential impacts on human health from operating the FBI without the GAC, GBMSD contracted with Short Elliot Hendrickson Inc. to conduct air dispersion modeling to calculate potential off-site mercury concentrations and to compare those potential impacts with state health-based standards. The ambient air quality standards for mercury are shown in the Wisconsin Administrative Code, NR 445, Table A.

These standards are a 24-hour average<sup>2</sup> concentration of 0.6 micrograms per cubic meter ( $\mu$ g/m³) and an annual³ average concentration of 0.3  $\mu$ g/m³. The air dispersion modeling was conducted in accordance with Wisconsin Air Dispersion Modeling Guidelines and the federal Guideline on Air Quality Models (40 CFR 51 Appendix W). A memorandum documenting the air dispersion modeling completed is enclosed.

For evaluation of the 24-hour standard, the actual days the FBI has run without the GAC and is anticipated to run without the GAC (November 21, 2019 through January 31, 2020) were modeled using the 0.000646 lb/hr mercury emission rate. The resulting highest impact, 0.00187  $\mu$ g/m³ is about 0.3 % of the 24-hour standard.

<sup>&</sup>lt;sup>1</sup> The emission rate and emission concentration shown on this table are based on emission testing conducted at the GBMSD facility on December 12, 2019 without the operation of the GAC.

<sup>&</sup>lt;sup>2</sup> Wisconsin's 24-hour standard is 2.4% of the mercury TLV the American Conference of Governmental Industrial Hygienists.

<sup>&</sup>lt;sup>3</sup> Reference Concentration for Inhalation Exposure for mercury from EPA Integrated Risk Information System.

GBMSD I08 Emission Test without GAC (Mercury) Page 4 of 4 January 23, 2020

For the annual standard analysis, the FBI was modeled as "off for the shutdown period (October 19, 2019 through November 20, 2019), "on" at 0.000646 lb/hr during the actual days when the FBI operated or is anticipated to operate without the GAC (intermittently from November 21, 2019 through January 31, 2020), and then "on" at the permitted mercury concentration rate for the remainder of the 365 day period (February 1 through October 18, 2020). The resulting impact,  $0.00004 \,\mu\text{g/m}^3$  is about 0.01% of the annual standard.

Table 2 - Modeling Results Compared with Ambient Air Standards for Mercury

	Averaging Period	Modeled Concentration (µg/m³)	Ambient Standard (µg/m³)	% of Standard
	24-hr	0.00187	0.6	0.3%
-	Annual	0.00004	0.3	0.01%

While operating the FBI without the GAC might exceed the allowable mercury concentration, modeling indicates that it does not pose a significant risk to the public. The air dispersion modeling evaluation demonstrates that the impacts from the emission rate are well within state health-based standards.

Please feel free to contact Julie Maas by phone at (920) 438-1045 or email at jmaas@newwater.us with any questions or comments you may have.

Sincerely,

**GREEN BAY METROPOLITAN** 

SEWERAGE DISTRICT

Thomas W. Sigmund, P.E.

**Executive Director** 

c. Louise Gross, US EPA
 Daniel Schaufelberger, US EPA
 James Bonar-Bridges, WDNR
 Thomas Henning, SEH

### Enclosures:

- 1: Advanced Industrial Resources Sewage Sludge Incineration Unit Emission Test Report Test Date December 12, 2019
- 2: SEH Technical Memorandum Analysis of impact of Mercury Emissions from FBI

1 Agmind



# SEWAGE SLUDGE INCINERATION UNIT EMISSION TEST REPORT FLUIDIZED BED INCINERATOR (FBI) PROCESS 108 – STACK S08 AT GREEN BAY METROPOLITAN SEWERAGE

GREEN BAY METROPOLITAN SEWERAGE
DISTRICT TREATMENT PLANT
PROJECT ID: KR-10375

PREPARED FOR:



# GREEN BAY METROPOLITAN SEWERAGE DISTRICT 2231 NORTH QUINCY STREET GREEN BAY, WISCONSIN 54302

PREPARED BY:

ADVANCED INDUSTRIAL RESOURCES, INC. 3407 Novis pointe
ACWORTH, GEORGIA 30101

TEST DATE: **DECEMBER 12, 2019** 

3407 NOVIS POINTE ACWORTH, GEORGIA 30101 V. 404.843.2100 F. 404.845.0020



"Greg Essig-

Field Project Supervisor

Advanced Industrial Resources

### REPORT CERTIFICATION SHEET

Having conducted the Technical Review of this repo	ort, I hereby certify the data,
information, results, and calculations in this report to	o be accurate and true according to
the methods and procedures used.	
Deruk - Store	January 15, 2020
Derek Stephens	Date
Technical Director	
Advanced Industrial Resources	
Having written and prepared this report, I hereby ce results in this report to be correct and all inclusive o for a complete third-party review of the testing even	f the necessary information required
Steen Hardy	January 15, 2020
Steven Haigh	Date
Report Preparation Director	

Having supervised all aspects of the field testing, I hereby certify the equipment preparation, field sample collection procedures, and all equipment calibrations were

January 15, 2020

Date

conducted in accordance to the applicable methodologies.

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# **APPENDICES**

APPENDIX A: TEST RESULTS

APPENDIX B: FIELD DATA REDUCTION

APPENDIX C: EXAMPLE CALCULATIONS AND NOMENCLATURE

APPENDIX D: FIELD DATA (SEE ATTACHED CD FOR COMPLETE MONITOR DATA)

APPENDIX E: LAB REPORTS

APPENDIX F: CALIBRATION DATA

APPENDIX G: PROCESS OPERATION DATA

### 1.0 INTRODUCTION

### 1.1 SUMMARY OF TEST PROGRAM

The Green Bay Metropolitan Sewerage District (GBMSD) operates the existing wastewater treatment plant located at 2231 North Quincy Street, Green Bay, Wisconsin. The facility operates a fluidized bed incinerator (FBI) to treat biosolids generated at the plant. The FBI is listed in the facility's air permit as Process I08 which vents to atmosphere via Stack S08. GBMSD operations are regulated under Wisconsin Department of Natural Resources (WDNR) Air Pollution Control Operation Permit No. 405004600-P30 and Construction Permit No. 14-JJW-051-R1. Those permits contain emission limits for mercury of 7.1 pounds per 24 hour period (0.296 lb/hr) and 0.0010 milligrams per dry standard cubic meter.

GBMSD proposed to conduct emission testing for mercury without the operation of a granular activated carbon system (GAC). The GAC was installed to control the emissions of mercury from GBMSD's FBI. In a letter dated August 1, 2018, the United States Environmental Protection Agency (US EPA) approved a request from GBMSD to operate the GAC only if needed to meet emission limits for mercury. If emissions of mercury from the FBI meet the compliance limits without the GAC, GBMSD has the option to combust sewage sludge without operating the GAC.

The purpose of this testing effort is to evaluate emissions of mercury from the FBI without use of the GAC. Testing was performed to measure mercury emissions. The GAC was not operated during testing. All other air pollution control units were operated during testing and their operating parameters were monitored and recorded.

Testing was conducted on December 12, 2019, in accordance with a Wisconsin DNR approved Site-Specific Test Protocol (SSTP). All testing was conducted by Advanced Industrial Resources, Inc. (*AIR*) in accordance with approved USEPA Methods (i.e., 40 CFR 60 Appendix A, Methods 1, 2, 3, 3A and 29).

### 1.2 KEY PERSONNEL

The key personnel who coordinated the test program and their telephone numbers are:

Julie Maas, Green Bay MSD

920-438-1045

Advanced Industrial Resources, Inc.

Green Bay Metropolitan Sewerage District, Green Bay Wisconsin Performance Test - 40 CFR 60 LLLL SSI & Permit Compliance Test Report - Project ID		Page 2 of 10
Bruce Bartel, Green Bay MSD	920-438-1	006
Thomas Henning, Short Elliot Hendrickson Inc.	920-287-0	677
Derek Stephens, Advanced Industrial Resources	404-843-2	100
Scott Wilson, Advanced Industrial Resources	800-224-5	007
Ross Winne, Advanced Industrial Resources	404-843-2	100
Steve Haigh, Advanced Industrial Resources	404-843-2	100

### 2.0 PROCESS AND SAMPLING LOCATION DESCRIPTIONS

### 2.1 PROCESS DESCRIPTION

The Green Bay Metropolitan Sewerage District (GBMSD) operates wastewater treatment plants in Green Bay and De Pere, Wisconsin. GBMSD implemented the Resource Recovery and Electrical Energy Project (R2E2) to replace its solid handling facility and meet the increased capacity of sludge from the De Pere Facility along with meeting the Subpart LLLL SSI standards. The facility receives and treats wastewater by screening, grit removal, primary clarification, and activated sludge treatment with biological phosphorus removal. The solids at the De Pere Facility are pumped to the Green Bay Facility where they are dewatered and incinerated, the resulting ash of which is landfilled.

The Fluidized Bed Incinerator (FBI) receives anaerobically digested, polymer conditioned, and centrifuge dewatered biosolids. The FBI system includes a biosolids dryer, incinerator feed pumps, a fluidized bed reactor, a hot thermal oil heat exchanger, a wet scrubber, a wet electrostatic precipitator, an exhaust gas conditioner and re-heater, a static bed carbon adsorber, blowers, fans, exhaust flues, and ducting. The FBI has a design sludge feed rate of 51 dry tons per day.

The operation of the FBI and the associated control equipment is monitored using flow monitors, combustion temperature, power inputs, scrubber liquid pH, effluent water flow rate, and pressure differential monitors for determining the pressure drop of gas flow across the scrubber. The exhaust of the FBI is also equipped with oxygen (wet and dry) and carbon monoxide continuous emissions monitoring systems (CEMS).

### 2.2 SAMPLING LOCATION DESCRIPTION

The exhaust Stack S08 of the FBI has a circular cross section with an internal diameter of 23.625 inches. The sampling locations are located at 15.2 equivalent diameters downstream from the nearest upstream flow disturbance and at 34.5 equivalent diameters upstream from the nearest downstream flow disturbance or stack exhaust. The stack has at least two sampling ports oriented 90 degrees to one another in a plane perpendicular to the flow direction. Twelve sampling points (six points per port) were used for USEPA Methods 2, 3, 4 and 29 sampling, in accordance with USEPA Method 1 requirements.

### 3.0 SUMMARY AND DISCUSSION OF TEST RESULTS

### 3.1 OBJECTIVES

The purpose of this testing effort is to evaluate emissions of mercury from the FBI without use of the GAC. Testing was performed to measure mercury emissions. The GAC was not operated during testing. All other air pollution control units were operated during testing and their operating parameters were monitored and recorded.

### 3.2 FIELD TEST CHANGES, PROBLEMS, & ITEMS OF NOTE

The testing was conducted in accordance with the associated Site-Specific Test Protocol submitted to Wisconsin DNR prior to testing and no problems were encountered during testing that required deviation from the planned test protocol.

### Items of Note:

Upon receipt of the sample shipping cooler at the analytical laboratory, it was noted by laboratory personnel that each of the respective runs' Sample container 5B's had lost liquid sample contents. Based upon the sample level markings placed on each of the respective sample containers prior to shipping and the method specified volumes of sample rinses, it is estimated that the volumes lost ranged from 40-90 mL.

As suggested in the Note listed after Method 29, Section 8.2.9.2, a pressure relief hole was used in the Container 5B cap to prevent excessive pressure build-up of the contents resulting from the potential reaction of potassium permanganate (KMnO<sub>4</sub>) with acid (0.1 N H<sub>2</sub>SO<sub>4</sub>).

The samples were shipped from the field to the contract laboratory via private courier (UPS). During shipment, the sample shipping cooler was apparently handled roughly. Therefore, while the sample bottles were sufficiently protected from breakage using packing materials (bubble wrap, etc.), the jostling of the container resulted in liquid sample being extricated from the respective Container 5B sample cap holes.

While the lab was able to estimate the quantities lost, they were not able to definitively determine the lost volumes. Therefore, the lab analyzed the samples 'as is' after diluting

the samples to 500 mL, as per normal sample analysis protocol. The analysis conducted is on a concentration basis whereby at least two (2) representative aliquots of the respective sample containers' contents are analyzed. The resulting concentrations (ug/mL) are then extrapolated to a total mass collected (ug) using the total volume (mL) of the sample from which the aliquot(s) were analyzed (ug<sub>Sample</sub> = ug/mL<sub>Aliquot</sub> x mL<sub>Total Volume</sub>). Therefore, while it is possible that some mercury was lost along with the liquid sample loss, the overall concentration of the sample containers' contents were likely unaffected. Additionally, because the samples were each diluted up to 500 mL prior to analysis, per normal protocol, the final calculated mass (ug) reported was likely unaffected and thus the emissions reported based upon the analytical results should be considered representative of the actual source emissions.

### 3.3 PRESENTATION OF TEST RESULTS

Emission test results are presented in Appendix A and are summarized in Table 3-1. Reduced and tabulated data from the field-testing is included in Appendix B. The calculations and nomenclature used to reduce the data are presented in Appendix C. Actual raw field data sheets are presented in Appendix D. Laboratory reports and custody records are presented in Appendix E. Equipment calibration information and Gas Calibration Certification sheets are presented in Appendix F. Facility process data, as provided, is included in Appendix G.

**TABLE 3-1: Results Summary** 

Source	Pollutant	Average Measured	Allowable	Units	% of Allowable	Regulatory basis
FBI	Mercury	0.0220	0.0010	mg/dscm @ 7%O <sub>2</sub>	2201%	40 CFR 60, Subpart LLLL
Stack 08	(Hg)	0.0155	7.1	lb/24-hour	0.2%	40 CFR 61, Subpart E

<sup>\*</sup> Measured hourly emission rate is 0.000646 lb/hour.

### 3.4 PROCESS MONITORING

All essential process monitoring equipment was operating properly and recording data throughout the test period.

Facility personnel collected sludge samples for applicable analysis within the GBMSD laboratory for determinations of sludge throughput processing rates. Analytical results and sludge feed rates are presented in Appendix G.

### 4.0 SAMPLING AND ANALYTICAL PROCEDURES

Testing was conducted according to the methodology in the *Title 40 Code of Federal Regulation*, Part 60, Appendix A as applicable. The following methods were employed for emission sampling and analyses:

- EPA Method 1 was used for the qualification of the location of sampling ports and for the determination of the number and positions of stack traverse points, as applicable to sample traverses for Method 2.
- EPA Method 2 was employed for the determination of the stack gas velocity and volumetric flow rate during stack sampling using the Type "S" Pitot tube.
- EPA Methods 3 and 3A were used for the calculation of the density and dry molecular weight of the effluent stack gas. An instrumental analyzer was used for the determination of molecular oxygen and carbon dioxide concentrations.
- EPA Method 4 was used for the determination of moisture content.
- EPA Method 29 was used for the determination of mercury emissions.

Emission and process samples, as applicable, were recovered on site in a controlled environment and stored in appropriate storage containers. The liquid level was marked to provide an indication of the loss of liquid sample during transport. Filters were placed and sealed in a Petri dish. All applicable samples were stored upright in closed sample boxes until final laboratory analysis. In order to limit the chain of custody, only essential *AIR* personnel are permitted access to these samples.

### 5.0 QUALITY ASSURANCE ACTIVITIES

The quality assurance/quality control (QA/QC) measures associated with the sampling and analysis procedures given in the noted EPA reference methodologies, in Subparts A of 40 *CFR* 60 and 40 *CFR* 63, and in the *EPA QA/QC Handbook*, Volume III (EPA 600/R-94/038c) were employed, as applicable. Such measures included, but were not limited to, the procedures detailed below.

### 5.1 PROBE NOZZLE DIAMETER CHECKS

Probe nozzles were calibrated before field testing by measuring the internal diameter of the nozzle entrance orifice along three different diameters. Each diameter was measured to the nearest 0.001 inch, and all measurements were averaged. The diameters were within the limit of acceptable variation of 0.004".

### 5.2 PITOT TUBE FACE PLANE ALIGNMENT CHECK

Before field testing, each Type S Pitot tube was examined in order to verify that the face planes of the tube were properly aligned, per Method 2 of 40 *CFR* 60, Appendix A. The external tubing diameter and base-to-face plane distances were measured in order to verify the use of 0.84 as the baseline (isolated) Pitot coefficient. At that time the entire probe assembly (i.e., the sampling probe, nozzle, thermocouple, and Pitot tube) was inspected in order to verify that its components met the interference-free alignment specifications given in EPA Method 2. Because the specifications were met, then the baseline Pitot coefficient was used for the entire probe assembly.

After field testing, the face plane alignment of each Pitot tube was checked. No damage to the tube orifices was noted.

### 5.3 METERING SYSTEM CALIBRATION

Every three months each dry gas meter (DGM) console is calibrated at five orifice settings according to Method 5 of 40 *CFR* 60, Appendix A. From the calibration data, calculations of the values of  $Y_m$  and  $\Delta H_{@}$  are made, and an average of each set of values is obtained. The limit of total variation of  $Y_m$  values is  $\pm 0.02$ , and the limit for DH<sub>@</sub> values is  $\pm 0.20$ .

Advanced Industrial Resources, Inc.

After field testing, the calibration of the DGM console was checked by performing three calibration runs at a single intermediate orifice setting that is representative of the range used during field-testing. Each DGM was within the limit of acceptable relative variation from  $Y_m$  of 5.0%.

### 5.4 TEMPERATURE GAUGE CALIBRATION

After field testing, the temperature measuring instruments on each sampling train was calibrated against standardized mercury-in-glass reference thermometers. Each indicated temperature was within the limit of acceptable variation between the absolute reference temperature and the absolute indicated temperature of 1.5%.

### 5.5 DATA REDUCTION CHECKS

AIR ran an independent check (using a validated computer program) of the calculations with predetermined data before the field test, and the AIR Team Leader conducted spot checks on-site to assure that data was being recorded accurately. After the test, AIR checked the data input to assure that the raw data had been transferred to the computer accurately.

### 5.6 EXTERNAL QUALITY ASSURANCE

### 5.6.1 TEST PROTOCOL EVALUATION

A Site-Specific Test Protocol was submitted to the Wisconsin DNR in advance of testing, which provided regulatory personnel the opportunity to review and comment upon the test and quality assurance procedures used in conducting this testing.

### 5.6.2 ON-SITE TEST EVALUATION

A test schedule was submitted with the Site-Specific Test Protocol. No tests were performed earlier than stated in the original schedule. Therefore, regulatory personnel were afforded the opportunity for on-site evaluation of all test procedures. Mr. Andrew Seeber of Wisconsin Department of Natural Resources observed testing.

Advanced Industrial Resources, Inc.

### 6.0 DATA QUALITY OBJECTIVES

The data quality objectives (DQOs) process is generally a seven-step iterative planning approach to ensure development of sampling designs for data collection activities that support decision making. The seven steps are as follows: (1) defining the problem; (2) stating decisions and alternative actions; (3) identifying inputs into the decision; (4) defining the study boundaries; (5) defining statistical parameters, specifying action levels, and developing action logic; (6) specifying acceptable error limits; and (7) selecting resource-effective sampling and analysis plan to meet the performance criteria. The first five steps are primarily focused on identifying qualitative criteria such as the type of data needed and defining how the data will be used. The sixth step defines quantitative criteria and the seventh step is used to develop a data collection design. In regards to emissions sampling, these steps have already been identified for typical monitoring parameters.

Monitoring methods presented in 40 *CFR* 60 indicate the following regarding DQOs: Adherence to the requirements of this method will enhance the quality of the data obtained from air pollutant sampling methods. At a minimum, each method provides the following types of information: summary of method; equipment and supplies; reagents and standards; sample collection, preservation, storage, and transportation; quality control; calibration and standardization; analytical procedures, data analysis and calculations; and alternative procedures. These test methods have been designed and tested according to DQOs for emissions testing and analysis.

# APPENDIX A

**TEST RESULTS** 

### **Test Results**

Green Bay MSD Green Bay, WI FBI Stack S08

### Notes:

- 1) tpy-tons per year assumes continuous operation or 8,760 hours per year.
- 2) Permit FOP No. 405004600-P30 Emission limits
- 3) 40 CFR 60 LLLL New SSI Emission limits Table 1
- \* "Less than' symbol ( < ) indicates analyte of interest below the analytical detection limit; values reported based upon lab's detection limit

		Units	Run 1	Run 2	Run 3	Averages
Test Date			12-Dec-19	12-Dec-19	12-Dec-19	
	Start Time		7:00	10:25	13:50	
	End Time		10:03	13:29	16:54	
$\mathbf{P}_{\mathbf{m}}$	Pressure of meter gases	inches Hg	29.79	29.79	29.79	29.79
$P_s$	Pressure of stack gases	inches Hg	29.65	29.65	29.65	29.65
V <sub>m(std)</sub>	Volume of gas sample	dscf	109.58	106.00	110.83	108.81
V <sub>w(std)</sub>	Volume of water vapor	scf	2.17	2.27	2.41	2.28
$\mathbf{B}_{\mathbf{ws}}$	Moisture in stack gas		0.019	0.021	0.021	0.021
B <sub>ws,theo</sub>	Theoretical max. moisture	dimensionless	0.093	0.096	0.097	0.095
Bws,act	Actual moisture		0.019	0.021	0.021	0.021
$M_d$	Mol. Wt. Of gas at DGM	lb./lbmole	30.06	30.05	29.99	30.03
$\mathbf{M}_{\mathrm{s}}$	Mol. Wt. Of gas at stack	lb./lbmole	29.82	29.80	29.74	29.79
$\mathbf{V}_{\mathbf{s}}$	Velocity of stack gas	ft./sec	51.38	50.83	51.62	51.28
$\mathbf{A_n}$	Area of nozzle	ft <sup>2</sup>	0.000218	0.000218	0.000218	0.000218
$A_s$	Area of stack	ft <sup>2</sup>	3.04	3.04	3.04	3.04
Gas St	ream Flow Rates					
$Q_a$	Vol. Flow rate of actual gas	cfm	9,385	9,284	9,429	9,366
$Q_{sd}$	Vol. Flow rate of dry gas	dscfm	8,417	8,298	8,421	8,379
1	Isokinetic sampling ratio	percent	100.9	99.0	102.0	100.7
Gas St	ream Mercury Conce	ntrations				
$c_{Hg}$	Conc. Of Hg in dry stack gas	mg/dscm	0.0189	0.0208	0.0221	0.0206
c' <sub>Hg</sub>	Hg Conc. Corr. to 7% O <sub>2</sub>	mg/dscm @ 7%O <sub>2</sub>	0.0195	0.0219	0.0246	0.0220
c'Hg, All	Allow. Hg Conc. <sup>3</sup>	mg/dscm @ 7%O <sub>2</sub>	0.0010	0.0010	0.0010	0.0010
% of A	% of Allowable	%	1953%	2194%	2456%	2201%
$c_{Hg}$	Conc. Of Hg in dry stack gas	10 <sup>-6</sup> gr/dscf	8.23	9.06	9.66	8.99
Mercury Mass Rates						
E.	F	lb/hour	0.000594	0.000645	0.000697	0.000646
$\mathbf{E}_{\mathbf{Hg}}$	Emission rate of Hg	lb/24-hour	0.0143	0.0155	0.0167	0.0155
E <sub>Hg</sub> All	Allowable Hg Em. Rate	lb/24-hour <sup>2</sup>	7.1	7.1	7.1	7.1
	% of Allowable	%	0.2%	0.2%	0.2%	0.2%
$\mathbf{E}_{\mathbf{Hg}}$	Emission rate of Hg	tpy <sup>1</sup>	2.6E-03	2.8E-03	3.1E-03	2.8E-03

# APPENDIX B FIELD DATA REDUCTION

### **Data Reduction Sheet**

**Console ID: Client:** Green Bay MSD C-10 Green Bay, WI  $\mathbf{Y}_{\mathbf{m}}$ : 0.985 Location: FBI Stack S08  $\Delta H_{\widehat{a}}$ : Source: 1.825 SS, JG, GE  $C_p$ : Test Team: 0.84 **EPA Methods:** 1, 2, 3A, 4 & 29 Analyte(s): Hg

		Units	Run 1	Run 2	Run 3
Test Date			12-Dec-19	12-Dec-19	12-Dec-19
	Start Time		7:00	10:25	13:50
	End Time		10:03	13:29	16:54
$V_{\rm m}$	Volume of gas sample	def	114.390	111.513	116.475
$M_{lc}$	Mass of liquid collected	g	45.9	47.9	50.9
Δр	Velocity head of stack gas	inches H <sub>2</sub> O	0.792	0.773	0.795
$(\Delta \mathbf{p})^{1/2}$	Square root of velocity head	(inches H <sub>2</sub> O) <sup>1/2</sup>	0.890	0.879	0.891
ΔΗ	Pressure differential	inches H <sub>2</sub> O	1.27	1.24	1.27
θ	Total sampling time	minutes	180.0	180.0	180.0
$\overline{\mathbf{D}}_{\mathbf{n}}$	Diameter of nozzle	inches	0.200	0.200	0.200
$\mathbf{D}_{\mathbf{s}}$	Diameter of stack	inches	23.625	23.625	23.625
$T_{\rm m}$	Temperature of meter	°R	541	545	544
$T_s$	Temperature of stack gas	°R	572	573	573
$\mathbf{P}_{\mathrm{bar}}$	Barometric pressure	inches Hg	29.70	29.70	29.70
$\mathbf{p_g}$	Gauge pressure of stack gas	inches H <sub>2</sub> O	-0.70	-0.70	-0.70
% O <sub>2</sub>	Percent O2 by volume	percent ( <sup>v</sup> / <sub>v</sub> )	7.480	7.749	8.386
% CO <sub>2</sub>	Percent CO2 by volume	percent ( <sup>v</sup> / <sub>v</sub> )	10.998	10.865	10.352
% N <sub>2</sub>	Percent N2 by volume	percent (v/v)	81.5	81.4	81.3
$m_{\mathrm{Hg}}$	Mass of mercury	mg	0.0585	0.0623	0.0694

# APPENDIX C EXAMPLE CALCULATIONS & NOMENCLATURE

### Sample Calculation Sheet (Hg)

### Green Bay MSD, Green Bay, WI FBI Stack S08, Run #1

### Area of nozzle:

$$A_n = 3.1415 \times D_n^2 / 4 / 144 \text{ in}^2/\text{ft}^2$$

$$A_n = 3.1415 \times (0.2) \times (0.2) / 4 / 144$$

$$A_n = 0.000218$$
 ft<sup>2</sup>

### Area of stack:

$$A_s = 3.1415 \text{ x Ds}^2 / 4 / 144 \text{ in}^2/\text{ft}^2$$

$$A_s = 3.1415 \times (23.5) \times (23.5) / 4 / 144$$

$$A_s = 3.05$$
 ft<sup>2</sup>

### Absolute pressure of meter gases:

$$P_{\rm m} = P_{\rm bar} + \mathcal{O}_{\rm H} / 13.6$$

$$P_{\rm m} = 29.7 + 1.267 / 13.6$$

$$P_m = 29.79$$
 inches Hg

### Absolute pressure of stack gases:

$$P_s = P_{bar} + p_g / 13.6$$

$$P_s = 29.7 + -0.7 / 13.6$$

$$P_s = 29.65$$
 inches Hg

### Volume of gas sample, standardized:

$$V_{m(std)} = V_m \times Y_m (T_{std} / T_m) (P_m / P_{std})$$

$$V_{\text{m(std)}} = (114.39) \times (0.985) \times (528/541) \times (29.79/29.92)$$

$$V_{m(std)} = 109.49$$
 dsc:

### Volume of water vapor in the gas sample, standardized:

$$V_{w(std)} = (V_{lc} \times p_w \times R \times T_{std}) / (M_w \times P_{std})$$

$$V_{w(std)}$$
= (46) x (0.002201) x (21.85) x (528) / (18 x 29.92)

$$V_{w(std)} = 2.17$$
 sc

### Volume proportion of water in the stack gas stream:

$$B_{ws} = V_{w(std)} / (V_{m(std)} + V_{w(std)})$$

$$B_{ws}$$
= (2.17 / (109.49 + 2.17))

$$B_{ws} = 0.0194$$

### Nitrogen content of gas at the DGM:

$$\%N_2 = 100\% - \%CO_2 - \%O_2 - \%CO$$

$$\%N_2 = 100\% - 11\% - 7.48\% - 0\%$$

$$\%N_2 = 81.5$$
 %

<sup>\*</sup>Note: Values may not agree exactly with results shown elsewhere in this report due strictly to rounding

### Sample Calculation Sheet (Hg)

### Green Bay MSD, Green Bay, WI FBI Stack S08, Run #1

### Molecular weight of gas at the DGM:

$$M_d = ((44 \text{ x \%CO}_2) + (32 \text{ x \%O}_2) + (28 \text{ x (\%N}_2 + \%\text{CO)}))/100\%$$

$$M_d = ((44 \times 11) + (32 \times 7.48) + (28 (81.5 + 0)))/100\%$$

$$M_d = 30.05$$
 lb/lb-mole

### Molecular weight of gas at the stack:

$$M_s = M_d (1 - B_{ws}) + M_w \times B_{ws}$$

$$M_s$$
= (30.05 x (1 - 0.0194)) + (18 x 0.0194)

$$M_s$$
= 29.82 lb/lb-mole

### Velocity of stack gas:

$$v_s = K_p \times C_p \left[ \varnothing p \right]^{1/2} \times \left[ T_s / (P_s M_s) \right]^{1/2}$$

$$v_s = (85.49 \times 0.84 \times (0.792)^1/2 \times [572 / (29.65 \times 29.82)]^1/2$$

$$v_s = 51.40$$
 ft/s

### Volumetric flow rate of actual stack gas:

$$Qa = v_s \times A_s \times 60 \text{ sec/min}$$

$$Q_a = (51.4) \times (3.045384) \times (60 \text{ sec/min})$$

$$Q_a = 9392$$
 cfn

### Volumetric flow rate of dry stack gas, standardized:

$$Q_{sd} = (60 \text{ sec/min}) \times (1 - B_{ws}) v_s A_s (T_{std} / T_s) \times (P_s / P_{std})$$

$$Q_{sd} = (60 \text{ sec/min}) \times (1 - 0.0194) \times 51.4 \times 3.045384 \times (528 / 572) \times (29.65 / 29.92)$$

$$Q_{sd} = 8425$$
 dscfn

### Isokinetic sampling ratio expressed as percentage:

$$I= 100 T_{s} [(K_{3} \times V_{lc}) + (Y_{m} \times V_{m} \times P_{m} / T_{m})] / (60 \times Q \times V_{s} \times P_{s} \times A_{n})$$

$$I = 100 \times (572) \times ((0.002669 \times 46) + (0.985 \times 114.39 \times 29.79 / 541)))/(60 \times 180 \times 51.4 \times 29.65 \times 0.000218)$$

<sup>\*</sup>Note: Values may not agree exactly with results shown elsewhere in this report due strictly to rounding

### Sample Calculation Sheet (Hg)

### Green Bay MSD, Green Bay, WI FBI Stack S08, Run #1

### Concentration of Hg in dry stack gas, standardized:

 $c = (m_{Hg} / V_{m(std)}) (35.32 \text{ ft}^3 / \text{m}^3)$ 

 $c = (0.0585 / 109.49) \times 35.32$ 

c= 0.0189 mg/dscm

### Concentration of Hg in dry stack gas, standardized, Corrected to 7% O2:

 $\mathbf{c'} = \mathbf{c} * (20.9-7)/(20.9-\%O_2)$ 

 $\mathbf{c'} = (0.18871) \times (20.9-7)/(20.9-7.48)$ 

c'= 0.0195 mg/dscm corr  $7\%O_2$ 

### Concentration of Hg in dry stack gas, standardized:

 $c = (mg/dscm) / (35.32 ft^3 / m^3) / (64.8 mg/gr) x 1000000$ 

**c**= (0.018871) / 35.32 / 64.8\*1000000

 $c = 8.25 10^{-6} \text{ gr/dscf}$ 

### Emission rate of Hg, time basis:

 $E=\,c_{mg/dscm}\,x\;Q_{sd}\;x\;(60\;min/hr)\;x\;(2.2046\;x\;10^{-6}\;lb/mg)\,/\;(35.32\;ft^3\,/\;m^3)$ 

E= 0.018871 x 8425 x 60 x 2.2046 x 10-6 / 35.32

E= 0.000595 lb/hr

<sup>\*</sup>Note: Values may not agree exactly with results shown elsewhere in this report due strictly to rounding

### **EXAMPLE CALCULATIONS**

# Nomenclature

Symbol	Units	Description
Abs(x)	dimensionless	Absolute value of parameter x
An	ft <sup>2</sup>	Area of the nozzle
As	ft <sup>2</sup>	Area of the stack
Bws	dimensionless	Volume proportion of water in the stack gas stream
Cp	dimensionless	Type S pitot tube coefficient
Canalyte	mg/dscm	Concentration of analyte in dry stack gas, standardized
*Canalyte	gr./dscf	Concentration of analyte in dry stack gas, standardized
*Canalyte	ppm	Concentration of analyte in dry stack gas, standardized
CC	dimensionless	One-tailed 2.5% error confidence coefficient
d	ppm	Arithmetic mean of differences
di	ppm	Difference between individual CEM and reference
		method concentration value
Dn	inches	Internal diameter of the nozzle at the entrance orifice
Ds	inches	Internal diameter of the stack at sampling location
DE	percent	Destruction efficiency
$\Delta \mathbf{H}$	inches H <sub>2</sub> O	Average pressure differential across the meter orifice
$\Delta \mathbf{H}_{@}$	inches H <sub>2</sub> O	Orifice pressure differential that corresponds to 0.75
		cfm of air at 68 °F and 29.92 inches of Hg
$\Delta \mathbf{p}$	inches H <sub>2</sub> O	Velocity head of stack gas
Eanalyte	lb./hour	Emission rate of analyte, time basis
I	percent	Isokinetic sampling ratio expressed as percentage
Kı	dimensionless	K-factor, ratio of DH to DP, ideal
Kp	ft[(lb/lb-mol)(in.	Type S pitot tube constant,
	$[Hg]^{1/2}$	
	$s[(^{\circ}R)(in. H_2O)]^{1/2}$	= 85.49
Lp	cfm	Measured post-test leakage rate of the sampling train
Md	lb./lbmole	Molecular weight of gas at the DGM
Ms	lb./lbmole	Molecular weight of gas at the stack

# **NOMENCLATURE**

Symbol	Units	Description		
$M_{\rm w}$	lb./lbmole	Molecular weight of water,		
		= 18.0		
Manalyte	mg	Mass of analyte in the sample		
n	dimensionless	Number of data points		
P	MMBtu	Fuel firing rate		
P <sub>bar</sub>	inches Hg	Barometric pressure at measurement site		
Pinput	tons/hour	Process dry mass input rate		
Pg	inches H <sub>2</sub> O	Gauge (static) pressure of stack gas		
Pm	inches Hg	Absolute pressure of meter gases		
Ps	inches Hg	Absolute pressure of stack gases		
Pstd	inches Hg	Standard absolute pressure		
		= 29.92		
Qa	cfm	Volumetric flow rate of actual stack gas		
Qsd	dscfm	Volumetric flow rate of dry stack gas, standardized		
R	(in. Hg)(ft <sup>3</sup> )	Ideal gas constant,		
	(lb-mole)(°R)	= 21.85		
RA	percent	Relative accuracy		
RE	percent	Removal efficiency		
RM	ppm	Average reference method concentration		
rw	lb/mL	Density of water,		
		= 0.002201		
ra	g/mL	Density of acetone,		
		= 0.7899		
Sd	dimensionless	Standard deviation		
Tm	°R	Absolute temperature of dry gas meter		
Ts	°R	Absolute temperature of stack gas		
Tstd	°R	Standard absolute temperature,		
		= 528		
to.975	dimensionless	2.5 percent error t-value		
t <sub>m</sub>	°F	Temperature of DGM		
ts	°F	Temperature of stack gas		
θ	minutes	Total sampling time		

# **NOMENCLATURE**

Symbol	Units	Description	
Vlc	mL	Total volume of liquid collected	
V <sub>m</sub>	dcf	Volume of gas sample as measured by the DGM	
Vm(std)	dscf	Volume of gas sample as measured by the DGM,	
		standardized	
Vw(std)	scf	Volume of water vapor in the gas sample, standardized	
Vs	ft./sec	Velocity of stack gas	
Ym	dimensionless	DGM calibration coefficient	
Ye	dimensionless	DGM calibration check value	
Yw	dimensionless	Reference (wet) gas meter calibration coefficient	
% CO <sub>2</sub>	percent	Percent CO <sub>2</sub> by volume, dry basis	
% O2	percent	Percent O <sub>2</sub> by volume, dry basis	
% N <sub>2</sub>	percent	Percent N <sub>2</sub> by volume, dry basis	

# APPENDIX D

# FIELD DATA

SEE ATTACHED CD FOR COMPLETE MONITOR DATA

# **Advanced Industrial Resources, Inc.** Field Data Sheet

Client:	Green Bay MSD
Location:	Green Bay, WI
Source:	FBI Stack S08
Test Team:	SS, JG, GE
EPA Methods:	1, 2, 3A, 4 & 29
$D_s$ (in.):	23.625
% O <sub>2</sub>	7.480
% CO <sub>2</sub>	10.998
Start Run:	7:00 AM
End Run:	10:03 AM
Run Number:	1

Test Date:	December 12, 2019				
Console ID:	C-10				
$\mathbf{Y}_{\mathbf{m}}$ / $\Delta\mathbf{H}_{\mathbf{@}}$ :	0.985 1.825				
Sampling Box ID:	B-16				
Probe Assembly ID:	P4-01				
$\mathbf{D_n}$ (in.):	0.200				
Assumed B <sub>ws</sub> :	3.0				
P <sub>bar</sub> (in. Hg):		29.70			
$p_g$ (in. $H_2O$ ):	-0.70				
Minutes/Point:	15.0				
K-Factor:		1.6			

		Inches H <sub>2</sub> O		]	Temperature Readings (°F)				]		
Point	Meter (dcf)	Δр	ΔН	(\Delta p)^{1/2}	t <sub>s</sub>	Probe	Filter	Last Impinger	t <sub>m</sub> Average	Filter Exit	Vacuum (in. Hg)
1	803.250	0.75	1.20	0.866	110	249	248	57	77	N/A	2
2	812.83	0.77	1.23	0.877	112	251	252	57	77	N/A	2
3	821.70	0.80	1.28	0.894	111	250	250	58	77	N/A	2
4	831.37	0.81	1.30	0.900	112	251	248	60	77	N/A	2
5	841.92	0.79	1.26	0.889	110	250	248	60	79	N/A	2
6	851.81	0.78	1.25	0.883	111	251	250	61	80	N/A	2
7	861.25	0.75	1.20	0.866	111	249	250	61	80	N/A	2
8	870.92	0.78	1.25	0.883	112	250	249	62	81	N/A	2
9	880.58	0.78	1.25	0.883	113	251	250	62	81	N/A	3
10	889.99	0.82	1.31	0.906	114	264	263	62	86	N/A	3
11	898.35	0.82	1.31	0.906	114	269	263	61	86	N/A	3
12	907.18	0.85	1.36	0.922	114	258	263	60	86	N/A	3
End	917.640		<del></del>	•	<b>4</b>			•			•

Total Moisture Collected (mL): 46.0

Theoretical maximum moisture collection at saturation (ml): 239.0

Pre System Leak Check (cfm): 0.001

Post System Leak Check (cfm): 0.002

# **Advanced Industrial Resources, Inc.** Field Data Sheet

Client:	Green Bay MSD					
Location:	Green Bay, WI					
Source:	Incinerator 1					
Test Team:	SS, JG, GE					
EPA Methods:	1, 2, 3A, 4 & 29					
$D_s$ (in.):	23.625					
% O <sub>2</sub>	7.749					
% CO <sub>2</sub>	10.9					
Start Run:	10:25 AM					
End Run:	1:29 PM					
Run Number:	2					

Test Date:	December 12, 2019				
Console ID:	C-10				
$\mathbf{Y_m} / \Delta \mathbf{H_@}$ :	0.985 1.825				
Sampling Box ID:	B-16				
Probe Assembly ID:	P4-01				
$\mathbf{D}_{\mathbf{n}}$ (in.):	0.200				
Assumed B <sub>ws</sub> :	3.0				
P <sub>bar</sub> (in. Hg):		29.70			
$p_g$ (in. $H_2O$ ):	-0.70				
Minutes/Point:	15.0				
K-Factor:		1.6			

		Inches H <sub>2</sub> O				Temperature Readings (°F)					
Point	Meter (dcf)	Δр	ΔН	$(\Delta p)^{1/2}$	t <sub>s</sub>	Probe	Filter	Last Impinger	t <sub>m</sub> Average	Filter Exit	Vacuum (in. Hg)
1	917.751	0.77	1.23	0.877	111	244	262	62	82	N/A	2
2	926.91	0.78	1.25	0.883	113	253	263	62	82	N/A	2
3	936.23	0.76	1.22	0.872	113	253	263	56	83	N/A	2
4	945.71	0.76	1.22	0.872	113	253	260	54	84	N/A	2
5	954.92	0.80	1.28	0.894	113	250	260	53	85	N/A	2
6	964.59	0.80	1.28	0.894	113	250	261	54	86	N/A	2
7	973.22	0.73	1.17	0.854	114	251	261	55	86	N/A	2
8	982.88	0.71	1.14	0.843	114	252	262	55	86	N/A	2
9	992.47	0.80	1.28	0.894	114	253	260	55	85	N/A	2
10	1001.22	0.81	1.30	0.900	114	252	260	55	86	N/A	2
11	1010.89	0.78	1.25	0.883	113	252	260	56	86	N/A	2
12	1020.56	0.77	1.23	0.877	113	250	261	57	86	N/A	2
End	1029 264			•	·	•		•			

Total Moisture Collected (mL): 48.0

Theoretical maximum moisture collection at saturation (ml): 239.8

Pre System Leak Check (cfm): 0.001

Post System Leak Check (cfm): 0.002

# **Advanced Industrial Resources, Inc.** Field Data Sheet

Client:	Green Bay MSD					
Location:	Green Bay, WI					
Source:	FBI Stack S08					
Test Team:	SS, JG, GE					
EPA Methods:	1, 2, 3A, 4 & 29					
$D_s$ (in.):	23.625					
% O <sub>2</sub>	8.386					
% CO <sub>2</sub>	10.352					
Start Run:	1:50 PM					
End Run:	4:54 PM					
Run Number:	3					

Test Date:	December 12, 2019					
Console ID:	C-10					
Ym / DH@:	0.985 1.825					
Sampling Box ID:	B-16					
Probe Assembly ID:	P4-01					
Dn (in.):	0.200					
Assumed Bws:	3.0					
Pbar (in. Hg):	29.70					
pg (in. H2O):	-0.70					
Minutes/Point:	15.0					
K-Factor:		1.6				

		Inche	s H <sub>2</sub> O		Temperature Readings (°F)						
Point	Meter (dcf)	Δр	ΔН	$(\Delta p)^{1/2}$	t <sub>s</sub>	Probe	Filter	Last Impinger	t <sub>m</sub> Average	Filter Exit	Vacuum (in. Hg)
1	1029.365	0.86	1.38	0.927	114	240	260	62	80	N/A	2
2	1039.03	0.86	1.38	0.927	114	245	258	62	80	N/A	2
3	1048.38	0.80	1.28	0.894	113	250	258	62	82	N/A	2
4	1058.04	0.79	1.26	0.889	113	252	258	62	83	N/A	2
5	1067.70	0.79	1.26	0.889	113	250	258	63	84	N/A	2
6	1077.37	0.80	1.28	0.894	114	248	256	64	85	N/A	2
7	1086.09	0.78	1.25	0.883	114	244	263	64	85	N/A	2
8	1096.01	0.72	1.15	0.849	114	251	262	60	86	N/A	2
9	1106.65	0.78	1.25	0.883	113	253	260	60	86	N/A	2
10	1116.37	0.78	1.25	0.883	113	250	258	60	87	N/A	2
11	1129.98	0.80	1.28	0.894	113	256	260	59	86	N/A	2
12	1125.71	0.78	1.25	0.883	113	252	258	53	87	N/A	3
End	1145.840										

Total Moisture Collected (mL): 51.0

Theoretical maximum moisture collection at saturation (ml): 252.7

Pre System Leak Check (cfm): 0.002

Post System Leak Check (cfm): 0.001

# Cyclonic Flow Absence Verification Field Data EPA Method 1

Client:	Green Bay MSD			
Location:	Green Bay, WI			
Source:	FBI Stack S08			
Test Team:	SS, JG, GE			
Probe ID:	P4-01			
$C_p$ :	0.84			

Date:	October 12, 2019
D <sub>s</sub> (in.):	23.625
$A_s(ft^2)$ :	3.04
<b>D</b> <sub>n</sub> (in.):	0.200
$A_n (ft^2)$ :	0.000218

t <sub>m</sub> (°F):	71
Console ID:	C-10
$\mathbf{Y}_{\mathbf{m}}$ :	0.985
$\Delta \mathbf{H}_{@}$ :	1.825
Assumed B <sub>ws</sub> :	3%
P <sub>bar</sub> (in. Hg):	29.70

Point	Δp	α
1 OIIIt	(in. H <sub>2</sub> O)	(degrees)
1	0.0	0.0
2	0.0	0.0
3	0.0	5.0
4	0.0	0.0
5	0.0	0.0
6	0.0	0.0
C	hange Por	ts
1	0.0	0.0
2	0.0	0.0
3	0.0	5.0
4	0.0	0.0
5	0.0	0.0
6	0.0	0.0

# **Source Description Sheets**

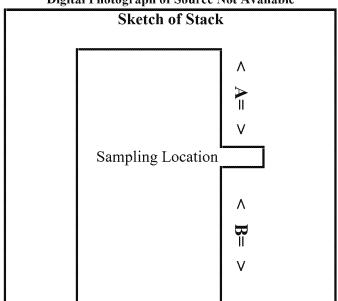
Client:	Green Bay MSD	
Location:	Green Bay, WI	
Source:	FBI Stack S08	

Date:	October 12, 2019		
Test Team:	SS, JG, GE		

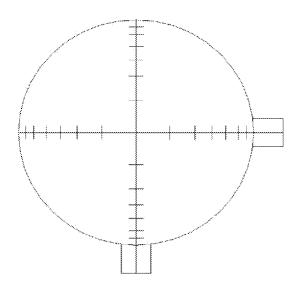
Source:	FBI Stack SU8	
***************************************		
<b>D</b> <sub>n</sub> (in.):	0.200	
$A_n$ (ft <sup>2</sup> ):	0.000218	
D <sub>s</sub> (in.):	23.625	
$A_s$ (ft <sup>2</sup> ):	3.04	
Length A:	> 47.3	
Length B:	> 189.0	
t <sub>amb</sub> (°F):	71	
Assumed B <sub>ws</sub> :	3%	
P <sub>bar</sub> (in. Hg):	29.7	
P <sub>g</sub> (in. H <sub>2</sub> O):	-0.70	
% O <sub>2</sub> :	9.0%	
% CO <sub>2</sub> :	10.0%	
Console ID:	C-10	
Y:	0.985	
ΔH <sub>@</sub> :	1.825	
C <sub>p</sub> :	0.84	
K-Factor:	1.6	

Point	Δp	t <sub>s</sub>		
	(in. H <sub>2</sub> O)	(°F)		
1	0.75	112		
2	0.80	110		
3	0.78	111		
4	0.78	113		
5	0.81	110		
6	0.82	112		
Change Ports				
1	0.83	113		
2	0.85	112		
3	0.85	113		
4	0.87	111		
5	0.86	114		
6	0.75	112		

Digital Photograph of Source Not Available



# Traverse Point Locations for Green Bay MSD FBI Stack S08



23.625 Inch Diameter Stack Two Ports at 90°

	Distance from
Sampling Point	Stack Wall (inches)
1	1.0
2	3.4
3	7.0
4	16.6
5	20.2
6	22.6

				Fie	eld Dat	a Sheet					
	Client:	breen	B. W	SD		Test Date:	12-12	.19			
	Location:	Green	13. 4.	150 NS 1 (50		Console ID:	6-10		The second secon	-	
	Source:	Incin	contur	1/50	(۶)	$Y_m / \Delta H_{@}$ :	0.985	1.425		•	
	Test Team:	SS, 50	, 68		Sampli	ng Box ID:	12.16			-	
	EPA Methods:	1-4,2	9		Decha Ac	sembly ID:			30001000110 1000 <del>11 1</del> 00101 11 11 11 11 11 11 11 11 11 11 11 1	•	
		73.5		25 PS	0)20		6.200			•	
	% O <sub>2</sub>	7.48				sumed B <sub>us</sub> :	3.%			-	
		10.99	g			bar (in. Hg):		·56 2	9.70	-	
	Start Run:		·			g (in. H <sub>2</sub> O):					
		10:63		***************************************	•	utes/Point:	00000000000000000000000000000000000000	·		-	
	Run Number:				•	K-Factor:			***************************************	•	
		***************************************		Т			<del>-</del>			<b>4</b>	ŀ
		Inche	s H <sub>2</sub> O			Tempera	ature Read	···	•	T	
	Meter						Last		m	Filter	Vacuun
Point	(def)	Δр	ΔĦ	t <sub>s</sub>	Probe	Filter Box	Impinger	Inlet	Outlet	Exit (M5 or CPM)	(in. Hg)
		6.00.0	1.0	14.0	0.14	71.0			7	1	
2	802. 25 813. 83	0.75	1.23	110	351 348	252	57 57	<del>77</del> 77	77 77	N/A	2
3	921.70	6.80	1.28	1///	250	250	37 (d)	<del>77</del> 77	77	N//A	2
4	831.37	0.81	1.30	11/2	251	340	20	17	77	N/A	2
5	841.92	0.79	1.2%	110	756	249	10	74	74	N/A	3
6	851.81	0.78	1.25		251	250	7.1	80	100	NIA	್ನ ಕ್ಷ
7		<u> </u>				1					
8											
9 -											
10				ļ							
11				ļ						ļ	
12					L Change	Danta	. :		<u> </u>	<u> </u>	<u> </u>
1	941.25	Δ ~~ /	1 2	Til	749	250	71	80	80	N/A	13
2	170.92	0.75	1.25	113	250	249	72	91	101	NA	3
3	180.58	0.71	1.25	113	231	250	7.5	l (i	81	N/A	3
4	१११ वर्ष	0.92	1.31	114	२८५	263	62	96	86	IV/A	3
5	998.35	6.82	).3]	114	269	12/3	71	86	86	N/k	3
6	907.10	0.83	1.36	1)4	254	37.3	60	86	86	N/14	3
7				'							
8											<u> </u>
9											
10				ļ	ļ					<b>-</b>	
11		<b> </b>				<del> </del>				<del> </del>	
End	917.640		L	1	1		<u> </u>	I	1	1	<u> </u>
	1 -11 // 0 -1 //		Moistur	e Collected (g	)		Pre-Run	Leak Checks	(defm @_"Hg	)	
		Initial	Final	Net	ĺ	San	pling Line:			•	
	Body:		436	36	1		Pitot A:		17		
	Silica Gel:	PROGRESSON	ী।0	10	1		Pitot B:		<i>f</i>		
	Gel Number:		Total	: 446	]		•		***************************************	<del></del>	
				•				Leak Checks	., -	()	
						San	ipling Line:		<u>(@. 5"</u>		
	011 0 10	C 11 1	Blue				Pitot A:		<b>/</b>		
	Silica Gel De		***************************************		,		Pitot B:	<u>v</u> _			
	Silica Gel D	-		<u>,                                    </u>	nae		11 .			lan e a	
	Test Team Lea	der Review:		10.		Reagent 1:	H202		Lot No:	19090	20G
	Data En	try Review:	10			Reagent 2:	H2504		Lot No:	141600	74
				·					-	17832	•
							KMIVO	λ			
							HN03			18075	•
							HLI			C58490	9
										="	

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C584461

Advanced Industrial Resources, Inc.									
Field Data Sheet									
Client: Green Boy MSD Test Date: 12-12-19									
Location:	(srcen	Bar	レエ		Console ID:	C-10	)		
Source:	Incin	Bay,	1 /508	)	$Y_m / \Delta H_{@}$ :	0.989	1 1.9	रेट	-
Test Team:	SS 5	(r , 6 G	( ,		ng Box ID:				-
EPA Methods:	1-4,	24		Probe As:	sembly ID:		4.114.114.114.14.14.14.14.14.14.14.14.14	788/IVITATE WILLA - 0 778 ALLE 1947	
D <sub>s</sub> (in.):	**********************	73.6	25 000	1/20	D <sub>n</sub> (in.):		······································		-
% O <sub>2</sub>		ANTONOMIA DE PARAMENTA ANTONOMIA			sumed B <sub>ws</sub> :	************************		<del></del>	•
% CO <sub>2</sub>			-M		ar (in. Hg):		<u> </u>		-
Start Run:	10:25				(in, H <sub>2</sub> O);				
End Run:	13:24			, `	utes/Point:	15	<u> </u>	aus	-
Run Number:	2 Cc.				K-Factor:	17			-
Turi Turi Del						1.0			-
	Inche	s H <sub>2</sub> O		Temperature Readings (°F)					
Meter						Last	t	m	Filter
(def)	Δр	ΔН	t <sub>s</sub>	Probe	Filter Box	Impinger	Inlet	Outlet	Exit (M5 or CPM)
917.751	0.77	1.23	1111	244	762	42	82	82	N/A
926.91	6.78	1.75	13	253	2(3	12	82	82	N/A
936.23 946.21	0.74	1.22	113	353	263	S'6	<u> </u>	<b>83</b>	N/A
354.42	0.80	1,72	113	253	360	54 C2	84 85	84	N/A N/A
964.59	0.80	1.28	113	250	261	54	85	45	NIA
112.89 36					,				
		,							

Point

10									<u> </u>		
11											
12											
					Change	Ports					
1	973. 22	0.73	1.17	114	751	12(1	55	16	86	NIA	7
2	982.88	0.71	1.12	1161	757	762	55	86	86	WIA	コ
3	912.47	0.80	1.28	114	253	360	5"5	85	85	W/A	しる
4	1001. 12	0.81	1.30	114	252	240	35	86	86	N/A	しる
5	1010.94	0.74	1-25	113	323	260	56	96	86	N/A	コ
6	1020.56	0.77	11.23	[13	320	7(1	57	86	86	N/A	2
7	_										
8											
9	-										
10											
11											
12											

End 1029.264 Moisture Collected (g) Initial Final Net 400 गउप Body: 214 Pitot B: Silica Gel: 200.0 Gel Number: Total: Post-Run Leak Checks (defm @ "Ho)

Data Entry Review:

		1 021-170	in Leak Checks	(acun @ 11g)
•		Sampling Lir	ie: 0.062	Ø 5''
	·O(	Pitot	A: ``	J/
Silica Gel Desc. (initial):	SIVL	Pitot	B: v	/
Silica Gel Desc. (final):		. 1		
Test Team Leader Review:	B	Reagent 1: 1-130	2	Lot No:

Reagent 1:	1-1202	Lot No:	14090204
Reagent 2:	H2504	Lot No:	19160071
•	KMNOH		178323
	HWO3		18075381
	1-166		6584461

Vacuum

(in. Hg)

# Field Data Sheet

Client:	Green Buy MSD	Test Date:	12-12-19
Location:	Green Bay WI	Console ID:	C-10
Source:	Incinenter 1 1508)	$Y_m / \Delta H_{@}$ :	0.985/1.825
Test Team:	56,55,6E	Sampling Box ID:	13-16
EPA Methods:	1-01,29 Pr	obe Assembly ID:	PU-0
D <sub>s</sub> (in.):	23-5 23.625 10/20	$D_{\alpha}$ (in.):	6.266
% O <sub>2</sub>	8.386	Assumed B <sub>ws</sub> :	3%
% CO <sub>2</sub>	10-352	P <sub>bar</sub> (in. Hg):	29.70
Start Run:	13:50	pg (in. H2O):	-6.76
End Run:	16:54	Minutes/Point:	15
Run Number:	3 Comp	K-Factor:	1.6

		Inche	s H <sub>2</sub> O			Tempera	ture Read	ings (°F)			
	Meter			***************************************			Last	t	m	Filter	Vacuum
Point	(def)	Δр	ΔH	t <sub>s</sub>	Probe	Filter Box	Impinger	Inlet	Outlet	Exit (M5 or CPM)	(in. Hg)
1	1029.365	0.86	1.38	114	240	240	62	80	80	N/A	a
2	1030.03	0.84	1.38	114	245	258	して	80	80	N/A	2
3	1049.38	6.80	1.28	)13	250	258	ζQ	82	82	N/A	2
4	1058.04	6.79	1,26	113	323	358	lΣ	83	83	N/4	る
5	101,7.70	0.79	1.76	[13	J20	328	63	84	84	NIA	2
6	10 77 37	0.80	1.78	114	248	<b>ゴ?</b> (	64	85	85	WIA	۵.
7								**********************			
<u>8</u>			***************************************		<u> </u>						
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10									ļ		
11			3000000.XX00000000000000000000000000000						· .		
12						<u> </u>				<u> </u>	
<u> </u>		I A = A		T 7.11	Change		7	85	1 1. 67	1 111 1	
1	1086.085	0.78	1.15	114	244	263	601	<u> </u>	45	N/A	스 -
3	1096.01	0.72	1.75	115	233	362	60	86	86	NIA	2
4	1116.65	0.78	1.25	113	250	258	60	07	0.7	N/A	2
5	1129.48	0.80	1, 28	113	236	360	39	86	86	NA	ష
6	1135.71	0.78	1 25	113	1352	258	53	83	8.7	NIA	3
7	,,,,,,,	10.10	1.35	1112	1,7,5,4	444	22	97	<del>  •</del>	1.70	
8				<b>†</b>	1	<u> </u>			<b></b>	<b>†</b>	
9					***************************************	1					
10									<u> </u>		
11											
12					1						
	10t15. 8410	<u> </u>	<del></del>	d				A			

Silica Gel Desc. (initial):
Silica Gel Desc. (final):

Test Team Leader Review:

Data Entry Review:

Pitot B:

Reagent 1:	11202	Lot No:	19690266
Reagent 2:	H2304	Lot No:	1916 0074
	KMNOu		178323
	HN03		1807538
	1-161		LS84961

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# Cyclonic Flow Absence Verification Field Data EPA Method 1

Client:	Green Bay MSD
Location:	Green Bay, WI
Source:	Incinerator 1 (508)
Test Team: _	54, JG, GE
Probe ID:	P4-01
C <sub>p</sub> : _	0.84

t <sub>m</sub> (°F):	<b>"1</b>
Console ID:	(-010
Y <sub>m</sub> :	0.985
ΔH <sub>@</sub> : _	1. 825
Assumed B <sub>ws</sub> :	3%
P <sub>bar</sub> (in. Hg):	90.70

Date:	10/12/19	1	
D <sub>s</sub> (in.):	23.5	23625	008
$A_s(ft^2)$ :	3-01	3.04	1/10/20
D <sub>n</sub> (in.):	0.200		
$A_n(ft^2)$ :	0.060872	*	

Point	Δp	α
	(in. H <sub>2</sub> O)	(degrees)
1	0.0	0
2	0.0	0
3	0.0	5
4	0.0	o
5	0.0	6
б	0.0	٥
C	hange Por	ts
1	0.0	0
2	0.0	0
3	0.0	5
4	0.0	U
5	0.0	Ó
6	0.0	Ö

Test Team Leader Review:

Data Entry Review:

# **Source Description Sheets**

	Source Beserve	CAUAL DIRECTO			
Client: 6	reen Bay MSD	Date:	10/1	2/19	
Location:	Green Bay, UT	Test Team:	Ss, J	6, GE	
Source:	Incineration 1 (508)			·	
	·	ſ	MILE STREET, MANAGEMENT STREET,		
D <sub>n</sub> (in.):	0.200		Point	Δp	t <sub>s</sub>
$A_n(ft^2)$ :	0.000872		1 01111	(in. H <sub>2</sub> O)	(°F)
D <sub>s</sub> (in.):	23.5 23.685 OF		1	0.75	112
A. (ft²):	3.04 3.04 1/10/20		2	0.80	110

D <sub>s</sub> (in.):	23.5	23.675	_0P
$A_s$ (ft <sup>2</sup> ):	3-0+	3.04	1/10
Length A (in.):	47	>47.3	
Length B (in.):	<del>1</del> 88	7 189.	0

t <sub>amb</sub> (°F):	71	
Assumed B <sub>ws</sub> :	3	
P <sub>bar</sub> (in. Hg):	21.70	
Pg (in. H2O):	- 0.70	
% O <sub>2</sub> :	9	
% CO <sub>2</sub> :	lo	
Console ID:	(-010	
Y:	0.985	
$\Delta H_{@}$ :	1.825	
ΔH <sub>@</sub> : C <sub>p</sub> :	0.84	
K-Factor:	1.6	licsy

Point	Δр	t <sub>s</sub>
	(in. H <sub>2</sub> O)	(°F)
1	0.75	112
2	0.80	110
3	0.78	111
4	0.78	113
5	0.81	110
6	0.82	112
(	Change Por	ts
1	0.83	113
2	0.85	112
3	0.85	113
4	0.87	111
5	0.86	114
6	0.75	112
	0.83	112

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	11	
	12-	
	_ <b> </b> 3	
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 1	1	

Sketch of Stack

Test Team Leader Review:

Data Entry Review:

# APPENDIX E LABORATORY REPORTS

3407 Novis Pointe Acworth, GA 30101

Project ID: Green Bay MSD

Mercury

EPA Method 29 Analysis

Analytical Report 34026



Element One, Inc. 6319-D Carolina Beach Rd., Wilmington, NC 28412 910-793-0128 FAX: 910-792-6853 e1lab@e1lab.com

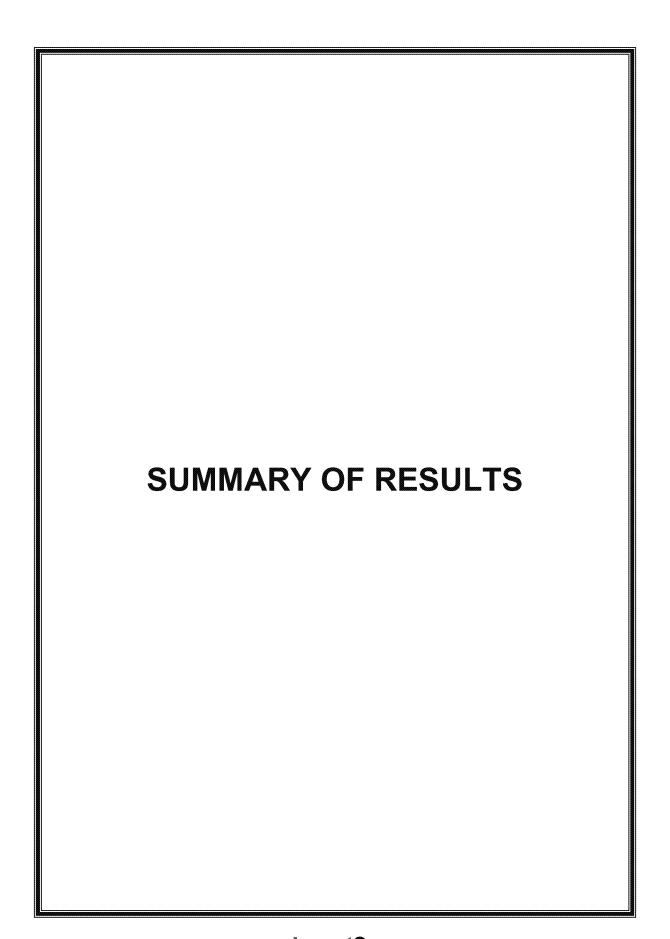
The following data for Analytical Report 34026 has been reviewed for completeness, accuracy, adherence to method protocol, and compliance with quality assurance guidelines.

Review by:

Katie Gattis, Quality Assurance Officer December 18, 2019

Report Reviewed and Finalized By:

Ken Smith, Laboratory Director December 18, 2019



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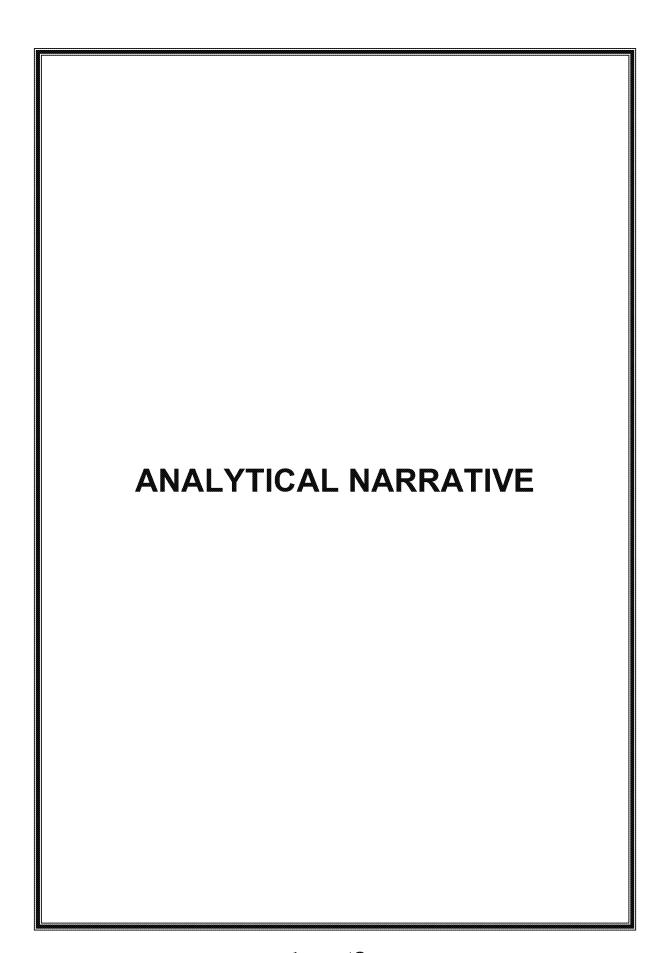
# **Summary of Analysis**

**Summary of Method 29 Mercury Analysis** 

Run Number		Average Total Catch, µg	Front Half µg	H <sub>2</sub> O <sub>2</sub> /HNO <sub>3</sub> µg	Empty Impinger µg	KMnO4 μg	HCI µg
Stack S08-M29-R1	#1	58.5	< 0.1	10.1	< 0.2	47.2	1.55
	#2		< 0.1	10.1	< 0.2	46.5	1.54
Stack S08-M29-R2	#1	62.3	< 0.1	10.3	< 0.2	49.5	2.64
	#2		< 0.1	10.2	< 0.2	49.5	2.62
Stack S08-M29-R3	#1	69.4	< 0.1	11.6	0.399	53.7	4.10
	#2		< 0.1	11.6	0.371	52.8	4.11
Reagent Blank	#1	< 0.5	< 0.1	< 0.2	< 0.2	< 0.5	< 0.4
	#2		< 0.1	< 0.2	< 0.2	< 0.5	< 0.4

#### elementOne

34026 AIR M29 Report Packet Page 4 of 22



#### **Element One Analytical Narrative**

Client:	Advanced Industrial Resources, Inc.	Element One #:	34026
Client ID:	Green Bay MSD	Analyst:	MAR
Method:	Method 29	Dates Received:	12/16/19
Analytes:	Hg	Dates Analyzed:	12/17-18/19

#### **Summary of Analysis**

The Method 29 samples were digested, prepared, and analyzed according to Method 29 protocol. Samples were analyzed for mercury on a PerkinElmer FIMS-100 CVAA mercury analyzer.

#### **Detection Limits**

The FIMS-100 CVAA instrument reporting limit for mercury was 0.004 µg per aliquot analyzed.

#### Analysis QA/QC

Duplicate analyses relative percent difference (RPD) and spike sample recovery data are summarized in the Quality Control Section. All QA/QC data was within the criteria of the method.

#### **Additional Comments**

The reported results have not been corrected for any blank values or spike recovery values. The reported results relate only to the items tested or calibrated.

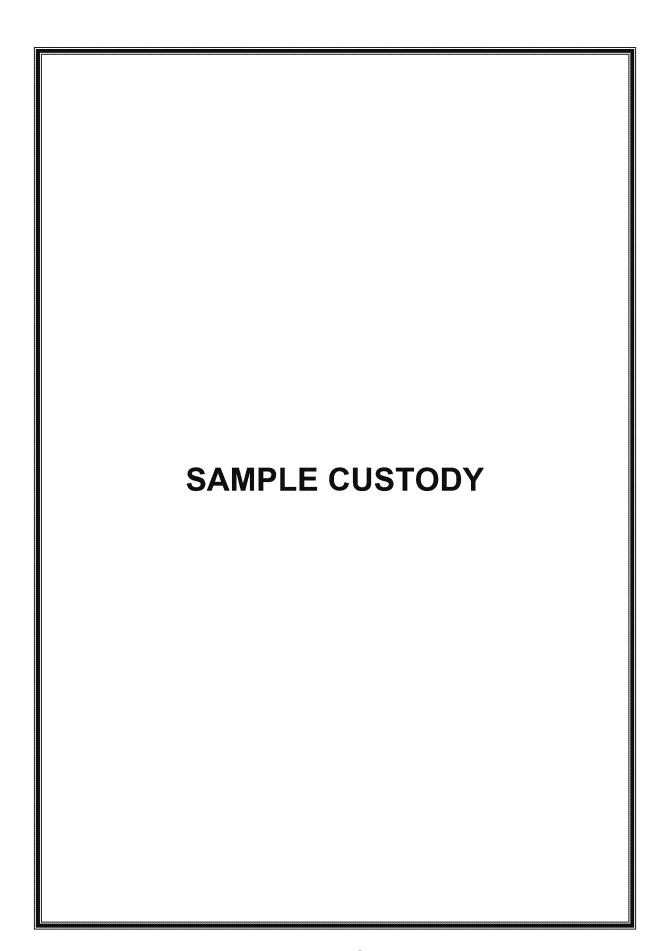
The KMnO<sub>4</sub> c5b fractions had leaked upon arrival. Using the volume marked line on the sample bottles, approximately 40-90mL sample was lost. Per client's instructions, samples were analyzed and prepared according to method protocol. Results may be biased for the KMnO<sub>4</sub> c5b fractions.



# **Summary of Quality Control Data**

# Mercury Duplicate Analysis RPD (Method 29 QC limits: < 10% for RPD)

Run Number	Fr	ont Half	H <sub>2</sub> O <sub>2</sub> /HNO <sub>3</sub>	Empty Imp	KMnO <sub>4</sub>	HCI
Stack S08-M29-R1	-	NA	0.4%	NA	1.4%	0.1%
Stack S08-M29-R2		NA	0.6%	NA	0.1%	0.6%
Stack S08-M29-R3		NA	0.1%	7.4%	1.7%	0.3%
Reagent Blank		NA	NA	NA	NA	NA
			ury Spike Re Climits: 75-125% fo.			
Run Number		Front Hal	f H <sub>2</sub> O <sub>2</sub> /HNO	3 Empty Imp	KMnO <sub>4</sub>	HCI
Stack S08-M29-R3	#1	113%	101%	99%	111%	108%
	#2	112%	97%	99%	109%	111%



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		ARCHES Name		NA FIELD Superson:	,				My/Mga:	* 1222200		2.82	38 2282200	14 12/12/2019	322	2312/12/2019	18 12 12 22 20 18	## H22322018	8 (37.87.80)	12.12.001			2022200		22.22.80			2	
	(1)				Minimum management of the commence of the comm		2.38		2000		2	***	348 338	**************************************				******	·			**************************************	***	*****	× × × ×				Green Sey MSD
	843 3460				***************************************	8 8 8			30000000 300 / SQ.	200	30			30000			220000000000000000000000000000000000000					# P P P P P P P P P P P P P P P P P P P				71 Canada 3	23 ( Name )		
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	000000000000000000000000000000000000000	*	*	8330		inalyses ?				*	**	>x 	*	*	*	*	*	*	*	**	38 	36 	38 	*	*	***************************************	*		Method 25
		*30.793.483				Analyses To Se Fortunand		3																	_				Method 22
			•	8		**	L	ð												-						S			Sample Condition
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#### element**One**

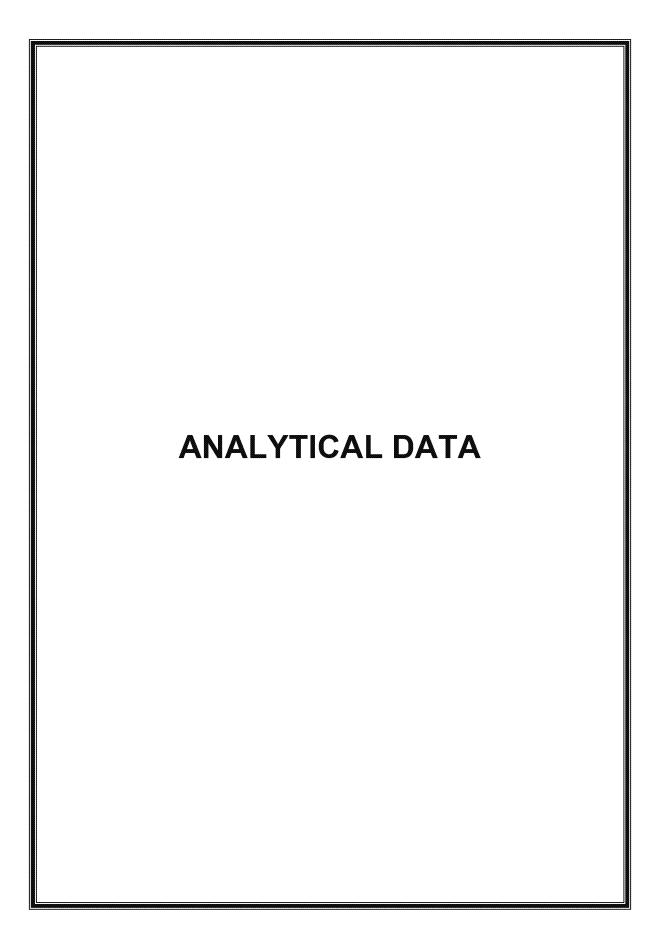
34026 AIR M29 Report Packet Page 10 of 22

# Advanced Industrial Resources, Inc. Compliance Sample Custody Record

A3K Coding Namber: (404) 843-2100					(404		280
	910-793-0128	**		Tank Stephens			AIR Contact Name
	W. 1988 12	*	***************************************		8	- X	Floor Supervisor Sign:
	8319437 Carolina Brack R4	8379	30000000000000000000000000000000000000				ALK FIRM DAY OF SHIP
Cana				***************************************	***************************************		
	Analyses to Be Feefer and By	**************************************	jā.			8000000	Fald Team Members
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<b>X</b>			Resinguished By / Steel Date/To	Received By Name			
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		-		\$0000000000000000000000000000000000000	***************************************		-
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		*	٠				- 8
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		*	Li	C	<u> </u>		i
						2	
	Sample Condition	Method 19 2 E			(3/8/ M8/ 3/8/)		8

### element**One**

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#### **Analytical Calculations**

#### Mercury-

Mercury Results ( $\mu$ g) = CVAA Results ( $\mu$ g) \*Final Volume (ml)
Aliquot (ml)

#### Where-

CVAA Results= Raw sample reading (µg)--Hg-Data Sheet

Aliquot= Sample Aliquot (Alq.)--Hg-Data Sheet

Final Volume=Final Volume (FV)\*--Sample Submission

\* With the exception of the BH fraction where-

=Received Volume (BV)--Sample Submission

# **Analytical Calculations**

#### Spike Recovery-

Spike (%) = (Spiked Result (
$$\mu$$
g/L) – Sample Result ( $\mu$ g/L)) X100  
Spike Amount ( $\mu$ g/L)

#### Where-

Spike Result = Raw sample concentration (ppb)--Hg-Data Sheet

Sample Result = Raw sample concentration (ppb)--Hg-Data Sheet

Spike Amount-- Hg-Data Sheet

#### **Duplicate Analysis RPD-**

RPD (%) = (Duplicate Result (
$$\mu$$
g/L) - Sample Result ( $\mu$ g/L)) X100  
Average ( $\mu$ g/L)

#### Where-

Sample Result and Duplicate Results=Raw sample concentration (ppb) -- Hg-Data Sheet

Average= (Duplicate + Sample Results)

2

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······································	e Identii tack S08-	000000000000000000000000000000000000000			4	Read	ent Siar	ık		<del></del>				
accomondance	itack S08-	M29-R2	•											
8	lack 508-	M29-R2 D	uplicate											
	itack S08-								*************					
- 5	itack S08-	M29-R3 S	pike			00000000000		,						
										1				
nalys	es Req	uested	Sample	is 1-4	Hg									
tuns /	Fu / A	ce (FH)	HNO	s JEPN	5% }			O2 (8H)	HN	Os ( <u>A)</u>		(پورە	HC	Я(Ω)
FB			p⊁i <2.	o(y/n		pH •	a.o (?)	) N	pH <2.		p#1 <2.	(V)N	<b>k</b> arania arang ar	0 (3)/N
.ab ID	FILIO	BV ml	8V mi	FV mi	8V n		Used	FV mi	BV mi	FV ml	BV mi	FV ml	8V ml	FV mi
	-	The state of the s	96	160	390	24			106	1900	<u>205</u>	<u> </u>	330	1400
.D .S			100	-	340 32	<u>.                                    </u>		<b>/</b>	10.2		340	<del></del>	2,25	+
			198	l	. seed be se	<b></b>		<u> </u>	llo-l	<u> </u>	ill)	Ľ <b>∀</b>		
a-29 R ab ID	i <b>cagent</b> Fractio	***********		.,,			8V, ml	FV, ml	Comm	ents				
C192 1 Ibr	C 7	T FH	Acetors	e Blank			23. 0. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2.		***************************************	***************************************		***************************************	***************************************	
	C 8A	FH	0.1N HI				60	100	W.) 6.	los	1 2 Km			
	C 8A	Α	0.1N HI	¥O3							***************************************		~	***************************************
	CaB	8	DIHO			C	140			3				
***********	Co	BH BH	. <del>,</del>	09/10% H			95	50	y Su		ML_		200	
	C 10	B   G	4% KM 8N HC	n0a/10%H	19 <b>0</b> Us		12 SH		20W	ארכיונ	) <u>+</u> 3(	s mol	CRR	
	C 12	FH	Filter				<u> </u>	900			***************************************			************
	ommuni	,,1,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	1 - 11-11					i_1907	daaa	**********************				***************************************
.au ∪c ∏		cauviis Kå W/(	1 J 3 2		i	63.3	11.12	<b>!</b> .!						
	:22.0.			<u> </u>	. 200, 200, 20		:::3.1.A.	~ <u>1</u> <u>1</u>	*****************	************		WARRANT TO THE PARTY OF THE PAR		20000000000000
						*******								
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													,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
		Runs; C1, C			9 8383		66 78 <b>0</b>	CO C10	C1112.1	6 15 W) /L				50000000000000000
5 600 000 000	rescensed.	194112, C1, S	(# <u>, 29, 50</u>	Transfer man	A	MES.A			COC TANGELLY	S-10-100.00				
										s ins				4
SS Pag	ge 1 of 1	non en e en e				FHP	rep By/	Date M	ar Idá	THE A	Prep By/D	late DKI	4 191	ودلعه
12/16/2	ឈាម 12:3	024 PM						Date <u>(Iky</u> By/Date		# C	Prep By/L Prep By/L	late Myn		11124)  11
53 For	11:220 *													

Lab ID # e 34024 Method 29 Microwave Worksheet elementOne Client: ATR Worksheet Prepared by: \_\_\_\_\_\_ Date Digested: <u>[기년]</u> \_\_\_\_ Initials: \_\_\_\_\_A-f Auto Prep Volume # of filters Sample Sample Lab ID Spike Comments digested (mi) Lac. LALS 100 BIN H LR3 \* 30026-1 1 10 HNO, Lot # (18/7) mLs Used: C

HF Lot # 5716072 mLs Used: Z

LR8 54 red W/01N 25445+3-4-3 021419-4

Element On	a. Inc.	F214	231	Microwave	Sheet M29

#### MERCURY BATCH DIGESTION - RUN WORKSHEET

Date Pr	epared/Digested:	1 Mir/La	Prep By:	purphables		SIF File #:	12,1419 -1		
	#1 Temperature:	93.28	Start Time:		w.	fachine ID:			
	#2 Temperature:	***************************************	Stop Time:		- Bat	ch Analyst:	***************************************		
	#3 Temperature:	*	Typed By:	gWa.		verified By:	777V 11		
***************************************		0.4ug/ml			1		<u> </u>		
A/S	Curve & QC's	working std		BV, ml	FV, mi	Standa	ard Lot Numbers		
					•	•	***************************************		
	Lab BLK					Standard	#1 (for working std		
1	(3/ batch)	0		40	40		04012 PU		
2	0.004 ug	0.01ml		40	40	Working S			
3	0.04 ug	0.10mi		40	40	Lot #: /%3-			
4	0.08 ug	0.20ml		40	40		#2 (QC #2):		
5	0.16 ug	0.40ml		40	40	Lot#: 14,3			
6	0.20ug	0.50ml		40	40	Standard #3 (QC #3):			
Lot #: (γ/ \-1))-3									
7	QC #2= 0.08ug	0.2ml #2 std		40	40	<b></b>	***************************************		
8	QC #3= 0.08ug	0.2ml #3 std		40	40	Curve prei	pared by: MAR		
						<b></b>	······································		
In	itial Review By: ∤^	N	***************************************	Di	ate: (᠘/۱ <del>)</del>	110	Time: to i 30		
Final	QC Review By: 1(	W)	***************************************		ite:  2  1	7117	Time: (\%)		
Commen	ts: <u> </u>	3.000	l mL						
***************************************	***************************************	/		***************************************			**************************************		
A/S	LAB#	Method	Wt (g)/ FV (mi.)	Prep Aliquot Used, mL	Asiguet or Calc Mass	FV, mL or "1" for conc.	Comments		
9	33593-18 BL	†4+oA			0.1	1	7V:5.3		
10	レ/レ	\ \			1	l,	€0.00\$		
11	3399>-2L	M <sub>23</sub>			4-	400	······································		
12	-1( p	1				V			
13	34026-19H			***************************************		20			
14						32.0			
	-784					340			
15						¥			
16						3,25			
17	~} OM +					V			
18	-† ð H					195	***************************************		
19	·····					200	***************************************		
	1.15	in beforestere en en esta en							
"+" Done	MUSSICO, Litt	J DISHINS SHU SJ	DIRES HIUSLD	a biabaiad	wan each	paich diges	NOR		
	NOTES: Lai des spike for Hg. Use n chemicals to be		0.4vg/mi stands	ird at the rate of	0.20mi per 4	Omi sample, ur	SION Hass otherwise noted.		
	2SO4 @ 2.0ml			-	*		te @ 3.2ml		
125041	.01# <u>531 15</u> #30.	rtHNO 3	Lof # 111(1)	g police	HCI i	Lot#: 415	lio Eige		
Persulfati	o Lot # <u>_14\$\*\\</u>	KMn	O , Lot #_# <u>_</u>	f. fal- E		lydrox Lot#	: Ny -144 - 8		
	Clear sa	mples after dig	estion with 2	2.4 ml of Hy	droxylamir	e solution.			
				***************************************	************************	**********************			

Element One, Inc F209 R9

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#### **MERCURY BATCH DIGESTION - RUN WORKSHEET**

SIF File #: 12 12 19-1

A/S	LAB#	Method	Wt (g)/ FV (mi.)	Prep Aliquot Used, ml.	Aliquet or Calc Mass	FV, mil. ox "1" for sons.	Comments
20	34026-28	WZ9			<b>4</b>	0.00	
21	-240	i			l	1	
22	-3 N						
23	~5 k.∤-						
24	-4A					1/	
25	- 13					5 a s	
26	-28					1	
27	-201						
28	-38						
29	~jo4						
30	-13	V			Ý	V	
31	34020-2	14474	10.5354/ya	4	0,642\$3	Į	
32	-2. ‡	•	0.3121 5.	Ţ.	0:040%	V	1420.1 mg
33							,
34		·					
35							
36						***************************************	·
37						***************************************	
38		***************************************				***************************************	
39		~~~~					
40							
41				***************************************			~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
42				•••••			
43		***************************************				•••••	
44							·····
45 46							
40 47		~~~~					
48							
49 49							
50							·····
51		***************************************					
52							•••••
53		······································					
54		***************************************					
:384	·····	***************************************					

Element One, Inc F209 R9

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#### MERCURY BATCH DIGESTION - RUN WORKSHEET

Date Pn	epared/Digested:	(2/18/19		MANARY		SIF File #:	12/8/19/4
	#1 Temperature:	43,36	Start Time:	5,745		fachine ID:	John Fr
	#2 Temperature:	- 13 to	Stop Time:	8:00		ch Analyst:	
Block	#3 Temperature:	94.06	Typed By:	} <b>\\</b> \.	ł	/erified By:	<u> DKH</u>
A/S	Curve & QC's	0.4ug/ml working std		BV, ml	FV, ml	Standa	rd Lot Numbers
	Lab BLK						#1 (for working std)
1	(3/ batch)	0		40	40		17882 AICLA
2	0.004 ug	0.01ml		40	40	Working S	
3	0.04 ug	0.10ml		40	40	Lot #: 1/g3-	
4	0.08 ug	0.20ml		40	40		#2 (QC #2):
5	0.16 ug	0.40ml		40	40	Lot #: [\1]	
6	0.20ug	0.50ml		40	40	<b>\$</b> ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	#3 (QC #3):
***************************************						Lot #: 1/47	-UT-}
<u></u>	QC #2= 0.08ug	0.2ml #2 std		40	40		**************************************
8	QC #3= 0.08ug	0.2ml #3 std		40	40	Curve pre	pared by: ***
B.o.	itial Review By: <sup>NA</sup>			L			77° / 200 - 200 /
		<u> </u>	<del></del>		ate: [\////		Time: 2:00
Commen		<u> </u>		DE	<u> </u>	<del> </del>	Time: \50 <u>0</u> )
Commen	10.						
A/S	LAB#	Method	Wit (g)/ FV (ml.)	Prep Aliquot Used, ml.	Aliquot or Calc Mass	FV, ast, or "1" for conc.	Comments
9	53393-18 00	74701			ø.(	3	t0=5.3
10	し/に	V			(	<b>\</b>	± 0.0 v}
11	34026 CROEN	M <sub>2</sub> .9			4	{o\$	
12	-(£3 t#.÷				1,6	1	
13			***************************************		4.		
14				,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			
15							
16				***************************************			
17							
18							
19		₩			1	500	***************************************
	1 3	b blanks and s	nikae muet h	w nanarad	with pach	the contract of the contract o	etion
"+" Denc	stes spike for Hg, Use						
Diaestio	n chemicals to b	e added in ord	ler at the fo	llowing rate	per 40mi	volumes.	
_	1 <sub>2</sub> SO 4 @ 2.0ml			-	•		le @ 3.2ml
	.0(# 14!!!) Preligion					Lot #: 411 <b>%</b> 1	
97	e Lot # 1/23-142-		***************************************				
		imples after dig					
							12an 1 1 3
Ele	ment One, Inc F209 I	<b>*</b> 83					Page 1 of )

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#### **MERCURY BATCH DIGESTION - RUN WORKSHEET**

SIF File #: 121819-1

			iiiii	Wt (g)/ FV	Prep Aliquot	Aliquot or	20.7	not no 649	
A/S	LAB#	Met		(mi.)	Used mi.	Calc Mass	fo	r conc.	Comments
20		<b>/</b> \2	9			f	15	03	
21	-231	1	000000000000000000000000000000000000000						
22	- 3 %							*******************************	
23	-304					V		1	
24	2 6					4	40	19	
25	~2 <u>6</u>					1			
26	-2 C Ø								
27	3 L								
28	-3 C +								
29		V				√		į	
30	-* ( <del>\$21 010 6</del> 1 511 1	74701	λ,			2.0			34029-030 Blk
	4 1/1,010-610 <b>4</b> 5	1				l		}	
¥	3 <b>4</b> 021-1								
33	***************************************								
34	~304								
35	~}								
36	-3 +								
37	4		••••						
38	-5								
39	-4								
40	~ }								
41	-8								
42	-9								
43	-10								
	<b>4028</b> - 1 //p	le le							
45	34028-2								
46	-204								
47	- 7								
48	<u>-3 ₹</u>								
49	-+								
50	~ <u>}</u>								
51	-6								
52	~ }								
53	~ 3								
54	- 1	V				1		$V \mid$	ţ

Element One, Inc F209 R9

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#### elementOne MERCURY BATCH DIGESTION - RUN WORKSHEET

SIF File #: [2-48]9-1

A/S	LAB#	Method	Wt (g)/ FV (mL)	Prep Aliquot Used, mL	Aliquot or Calc Mass	FV, mil. or *1* for conc.	Comments
	3 <b>6,63,</b> 8 - 10	440	38167	e erossa, nn.	2.0	l la cass.	CONTRIBUTES
56	3 <b>4</b> 029	111777			1	<u> </u>	
57	3 <b>4</b> 029 +	<del>                                     </del>			<del>                                     </del>	<del>                                     </del>	
58	2 <b>\$</b> 030				<del>                                     </del>	H	
59		<del>                                     </del>					
60	2867.2. e.k.)	7	<del>                                     </del>		<del>  Y                                   </del>	<u> </u>	
61							
62							
63							
64	•••••						
65						<b></b>	
66	····						
67							
68		<u> </u>					
69							
70	•••••	<b>*</b>	•				
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72	<del></del>						
73		······					
74						***************************************	
75	***************************************	***************************************					
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85		•	•				
86			***************************************	•	***************************************		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
87							
88							
89	***************************************	<b>*************************************</b>	<b>1</b>				

Eleme	ent One, Inc F209 R9	Page 3 of <sup>3</sup>

Hg-Data 1 of 1

Sample_ID	Date	Time	Mean_Sig	Mean_Rd	Mean_Rt	Units	Alq.	Vol.	Sig 1	Reading-1	Result-1	Sig 2	Reading-2	Result-2	Cor. Coeff.
Calib Blank	12/17/2019	8:32:32 AM 8:34:13 AM				μg			0.00015965			0.00015189 0.00058369			
STD1 = .004ug STD2 = .04ug	12/17/2019					μg			0.00060404 0.00458848			0.00058569			
STD3 = .08ug	12/17/2019	8:37:39 AM				μg			0.00934971			0.00948037			
STD4 = .16ug STD5 = .2ug		8:39:33 AM 8:41:26 AM				μg μg			0.01906768 0.02411755			0.0190457 0.0239551			
Reagent Blank		8:43:18 AM		0.00013496	0.00013496	µg				0.00019962	0.00019962	8.40E-06	7.03E-05	7.03E-05	
0.004ug = DL				0.0045272											0.999875288
0.080ug = QC STD 3 0.080ug = QC STD 2				0.07891733		ha ha									0.999875288 0.999875288
Reagent Blank	12/17/2019			-0.0001483		μg					-0.0001673				0.999875288
34026-1 BH	12/17/2019			0.12611403		μg	4								0.999875288
34026-2 BH 34026-2 BH DUP				0.12025125 0.11979389		μg μg	4 4		0.01442594 0.01428802						0.999875288 0.999875288
34026-3 BH	12/17/2019			0.14261736		μg	4	325							0.999875288
34026-3 BH SPK				0.22184339		μg	4	325							0.999875288
0.004ug = DL 0.080ug = QC STD 2				0.00448784 0.08022271		μg μg									0.999875288 0.999875288
Reagent Blank	12/17/2019	9:17:23 AM	-5.58E-06	-4.67E-05	-4.67E-05	μg			5.35E-06	4.48E-05	4.48E-05	-1.65E-05			0.999875288
Calib Blank STD1 = .004ug		9:42:01 AM 9:43:43 AM				μg			0.00016692 0.00059383			0.00016853 0.00060226			
STD1 = .004ug		9:45:25 AM				ha ha			0.00039363			0.00000220			
STD3 = .08ug		9:47:08 AM				μg			0.00985932			0.00958375			
STD4 = .16ug STD5 = .2ug		9:49:03 AM 9:50:56 AM				μg μg			0.01975411 0.02406405			0.01979364 0.02394514			
Reagent Blank				0.00083013	0.00083013	μg				0.00073779	0.00073779		0.00092246	0.00092246	
0.004ug = DL				0.00458914		μg									0.999723303
0.080ug = QC STD 2 Reagent Blank				0.07909826		μg μg									0.999723303 0.999723303
34026-4 BH		9:59:46 AM	7.55E-05			μg	4	195			-0.0080326		-0.0002512		0.999723303
34026-1 A				0.00157126		μg	4								0.999723303
34026-2 A 34026-2 A DUP				0.00160225 0.00178419		µg µg	4 4								0.999723303 0.999723303
34026-3 A				0.00769974		μg	4								0.999723303
34026-3 A SPK				0.08705825		μg	4								0.999723303
34026-4 A 0.004ug = DL		10:10:15 AM 10:17:39 AM		-0.0014403 0.00446265		μg μg	4	200			-0.0703142 0.00431443				0.999723303 0.999723303
0.080ug = QC STD 2						μg					0.08228512		0.081827		0.999723303
Reagent Blank		10:21:14 AM	6.41E-05	0.000528	0.000528	μg	,	500			0.00043356				0.999723303
34026-4 B 0.004ug = DL		10:26:41 AM 10:31:59 AM		-0.0009497 0.00437198		μg μg	4	500			-0.1109887 0.00443253		-0.0010114 0.00431143		0.999723303 0.999723303
0.080ug = QC STD 3						μg									0.999723303
Reagent Blank Calib Blank		10:35:34 AM 9:17:47 AM	7.43E-05 9.39E-05	0.00061229	0.00061229	μg			6.81E-05 9.36E-05	0.00056109	0.00056109	8.06E-05 9.43E-05	0.00066349	0.00066349	0.999723303
STD1 = .004ug		9:19:29 AM				μg μg			0.00043065			0.00042846			
STD2 = .04ug		9:21:11 AM				μg			0.00459494			0.00449624			
STD3 = .08ug STD4 = .16ug		9:22:54 AM 9:24:49 AM				μg μg			0.00924555 0.0189007			0.00914083 0.01869914			
STD5 = .2ug		9:26:42 AM				μg			0.02387101			0.02364878			
Reagent Blank		9:28:34 AM	-6.44E-06	-5.46E-05	-5.46E-05	μg			1.26E-06	1.06E-05	1.06E-05		-0.0001199		
0.004ug = DL 0.080ug = QC STD 3				0.00363293		μg μg					0.00352275				0.999832936 0.999832936
0.080ug = QC STD 2						μg									0.999832936
Reagent Blank		9:35:44 AM		-0.0001105		μg			-2.02E-05		-0.0001712	-5.87E-06	-4.98E-05		0.999832936
Reagent Blank 0.004ug = DL		11:39:28 AM 11:41:10 AM		-8.35E-05 0.00450599	-8.35E-05 0.00450599	μg μg					0.00011109		-0.0002781 0.00452318		0.999832936
0.080ug = QC STD 3	12/18/2019	11:42:52 AM	0.01007941	0.08548439	0.08548439	μg			0.01012196	0.0858452	0.0858452	0.01003687	0.08512359	0.08512359	0.999832936
0.080ug = QC STD 2															0.999832936
Reagent Blank 34026 LRB FH		11:50:22 AM 11:55:42 AM		0.00033012 0.00029527			4	100			0.0004124 0.00764902				0.999832936 0.999832936
34026 LRB FH SPK	12/18/2019	11:57:26 AM	0.00792068	0.06725951	4.20371933	μg	1.6		0.00795125	0.06751878	4.21992351				0.999832936
34026-1 FH 34026-2 FH		11:59:10 AM 12:00:53 PM		0.0003889 9.91F-05	0.00972252 0.00247752		4 4	100 100			0.01184246 -0.0032564				0.999832936 0.999832936
34026-2 FH DUP		12:00:35 PM		0.00040731			4	100			0.01069852				0.999832936
34026-3 FH		12:04:17 PM	-7.52E-05	-0.0005543	-0.0138577	μg	4	100	-8.23E-05	-0.0006142	-0.0153541	-6.81E-05			0.999832936
34026-3 FH SPK 34026-4 FH		12:05:58 PM 12:07:51 PM		0.09012949 0.00032532		μg μg	4 4	100			0.00854474				0.999832936 0.999832936
0.004ug = DL				0.00417473		μg									0.999832936
0.080ug = QC STD 2						μg									0.999832936
Reagent Blank 34026-1 B		12:13:06 PM 12:14:48 PM	1.93E-06 0.01104307	1.64E-05 0.09374073	1.64E-05 46.8703628	μg	1	500			0.00012065 47.2051362				0.999832936 0.999832936
34026-2 B	12/18/2019	12:16:41 PM	0.01165834	0.09895893	49.4794651	μg	1				49.5059284				0.999832936
34026-2 B DUP				0.09791569			1								0.999832936
34026-3 B 34026-3 B SPK				0.10658947 0.19475414			1								0.999832936 0.999832936
34026-1 C	12/18/2019	12:24:18 PM	0.00181251	0.01545556	1.54555607	μg	4	400	0.00181345	0.01546349	1.54634918	0.00181158	0.01544763	1.54476296	0.999832936
34026-2 C				0.02632505			4								0.999832936
34026-2 C DUP 0.004ug = DL				0.02612305 0.00432993			4	400							0.999832936 0.999832936
0.080ug = QC STD 2	12/18/2019	12:34:35 PM	0.01022299	0.08670207	0.08670207				0.01024529	0.08689118	0.08689118	0.01020069	0.08651296	0.08651296	0.999832936
Reagent Blank			-1.85E-06			μg	4	400	9.80E-06	8.31E-05					0.999832936
34026-4 C 34026-3 C			-4.12E-06 0.00482597		0.00485573 4.10130008		4 4	400 400			0.0111857 4.09501506				0.999832936 0.999832936
34026-3 C SPK	12/18/2019	12:41:34 PM	0.01511378	0.12826478	12.826478	μg	4	400	0.0149771	0.12710557	12.7105574	0.01525046	0.12942399	12.9423985	0.999832936
0.004ug = DL 0.080ug = QC STD 2				0.00438648											0.999832936 0.999832936
Reagent Blank				-8.49E-05							-0.0001906		2.07E-05		0.999832936
-															





December 20, 2019

Julie Maas NEW Water 2231 N Quincy Green Bay, WI 54302

RE: Project: DEC 2019 Hg STACK TEST

Pace Project No.: 40200724

#### Dear Julie Maas:

Enclosed are the analytical results for sample(s) received by the laboratory on December 13, 2019. The results relate only to the samples included in this report. Results reported herein conform to the most current, applicable TNI/NELAC standards and the laboratory's Quality Assurance Manual, where applicable, unless otherwise noted in the body of the report.

If you have any questions concerning this report, please feel free to contact me.

Sincerely,

DVM

Steven Mleczko

steve.mleczko@pacelabs.com

(920)469-2436 Project Manager

Enclosures





Pace Analytical\*
www.pacelabs.com

1241 Bellevue Street - Suite 9 Green Bay, WI 54302 (920)469-2436

#### **CERTIFICATIONS**

Project: DEC 2019 Hg STACK TEST

Pace Project No.: 40200724

Pace Analytical Services Green Bay

North Dakota Certification #: R-150

1241 Bellevue Street, Green Bay, WI 54302 Florida/NELAP Certification #: E87948 Illinois Certification #: 200050 Kentucky UST Certification #: 82 Louisiana Certification #: 04168 Minnesota Certification #: 055-999-334 New York Certification #: 12064

Virginia VELAP ID: 460263
South Carolina Certification #: 83006001
Texas Certification #: T104704529-14-1
Wisconsin Certification #: 405132750
Wisconsin DATCP Certification #: 105-444
USDA Soil Permit #: P330-16-00157

Federal Fish & Wildlife Permit #: LE51774A-0

#### **REPORT OF LABORATORY ANALYSIS**

Green Bay, WI 54302

(920)469-2436



#### **SAMPLE SUMMARY**

Project: DEC 2019 Hg STACK TEST

Pace Project No.: 40200724

Lab ID	Sample ID	Matrix	Date Collected	Date Received
40200724001	RUN 1	Solid	12/12/19 10:00	12/13/19 08:45
40200724002	RUN 2	Solid	12/12/19 13:25	12/13/19 08:45
40200724003	RUN 3	Solid	12/12/19 16:50	12/13/19 08:45

#### **REPORT OF LABORATORY ANALYSIS**



#### **SAMPLE ANALYTE COUNT**

Project: DEC 2019 Hg STACK TEST

Pace Project No.: 40200724

Lab ID	Sample ID	Method	Analysts	Analytes Reported
40200724001	RUN 1	EPA 7471	AJT	1
		ASTM D2974-87	QJR	1
		EPA 160.4	JXM	1
		SM 2540G	JXM	1
40200724002	RUN 2	EPA 7471	AJT	1
		ASTM D2974-87	QJR	1
		EPA 160.4	JXM	1
		SM 2540G	JXM	1
40200724003	RUN 3	EPA 7471	AJT	1
		ASTM D2974-87	QJR	1
		EPA 160.4	JXM	1
		SM 2540G	JXM	1

#### **REPORT OF LABORATORY ANALYSIS**



#### **ANALYTICAL RESULTS**

Project: DEC 2019 Hg STACK TEST

Pace Project No.: 40200724

Date: 12/20/2019 08:58 AM

Sample: RUN 1 Lab ID: 40200724001 Collected: 12/12/19 10:00 Received: 12/13/19 08:45 Matrix: Solid

Results reported on a "dry weight" basis and are adjusted for percent moisture, sample size and any dilutions.

Parameters	Results	Units	LOQ	LOD	DF	Prepared	Analyzed	CAS No.	Qual
7471 Mercury	Analytical	Method: EPA	.7471 Prepara	ation Metho	od: EPA	A 7471			
Mercury	0.23	mg/kg	0.098	0.029	1	12/16/19 10:05	12/17/19 10:21	7439-97-6	1q,C4
Percent Moisture	Analytical	Method: AST	M D2974-87						
Percent Moisture	65.2	%	0.10	0.10	1		12/19/19 11:52		
160.4 Total Volatile Solids	Analytical	Method: EPA	160.4						
Total Volatile Solids	69.1	% (w/w)	0.10	0.10	1		12/17/19 08:43		
2540G Total Percent Solids	Analytical	Method: SM	2540G						
Total Solids	34.9	%	0.10	0.10	1		12/17/19 10:49		

#### **REPORT OF LABORATORY ANALYSIS**



#### **ANALYTICAL RESULTS**

Project:

Date: 12/20/2019 08:58 AM

DEC 2019 Hg STACK TEST

Pace Project No.: Sample: RUN 2

40200724

Lab ID: 40200724002

Collected: 12/12/19 13:25 Received: 12/13/19 08:45 Matrix: Solid

Results reported on a "dry weight" basis and are adjusted for percent moisture, sample size and any dilutions.

Parameters ————————————————————————————————————	Results	Units	LOQ	LOD	DF	Prepared	Analyzed	CAS No.	Qual		
7471 Mercury	Analytical Method: EPA 7471 Preparation Method: EPA 7471										
Mercury	0.21	mg/kg	0.084	0.025	1	12/16/19 10:05	12/17/19 10:28	7439-97-6	1q,C4		
Percent Moisture	Analytical Method: ASTM D2974-87										
Percent Moisture	63.7	%	0.10	0.10	1		12/19/19 11:52				
160.4 Total Volatile Solids	Analytical Method: EPA 160.4										
Total Volatile Solids	69.3	% (w/w)	0.10	0.10	1		12/17/19 08:44				
2540G Total Percent Solids	Analytical Method: SM 2540G										
Total Solids	35.5	%	0.10	0.10	1		12/17/19 10:49				

#### **REPORT OF LABORATORY ANALYSIS**



#### **ANALYTICAL RESULTS**

Project:

Date: 12/20/2019 08:58 AM

DEC 2019 Hg STACK TEST

Pace Project No.:

Sample: RUN 3

40200724

Lab ID: 40200724003

Collected: 12/12/19 16:50 Received: 12/13/19 08:45 Matrix: Solid

Results reported on a "dry weight" basis and are adjusted for percent moisture, sample size and any dilutions.

Parameters ————————————————————————————————————	Results	Units	LOQ	LOD	DF	Prepared	Analyzed	CAS No.	Qual		
7471 Mercury	Analytical Method: EPA 7471 Preparation Method: EPA 7471										
Mercury	0.28	mg/kg	0.090	0.027	1	12/16/19 10:05	12/17/19 10:31	7439-97-6	1q,C4		
Percent Moisture	Analytical Method: ASTM D2974-87										
Percent Moisture	62.9	%	0.10	0.10	1		12/19/19 11:52				
160.4 Total Volatile Solids	Analytical Method: EPA 160.4										
Total Volatile Solids	69.3	% (w/w)	0.10	0.10	1		12/17/19 08:44				
2540G Total Percent Solids	Analytical Method: SM 2540G										
Total Solids	36.2	%	0.10	0.10	1		12/17/19 10:49				

#### **REPORT OF LABORATORY ANALYSIS**



**QUALITY CONTROL DATA** 

Project: DEC 2019 Hg STACK TEST

Pace Project No.: 40200724

Date: 12/20/2019 08:58 AM

QC Batch: 343458 Analysis Method: EPA 7471

QC Batch Method: EPA 7471 Analysis Description: 7471 Mercury

Associated Lab Samples: 40200724001, 40200724002, 40200724003

METHOD BLANK: 1994298 Matrix: Solid

Associated Lab Samples: 40200724001, 40200724002, 40200724003

Blank Reporting

Parameter Units Result Limit Analyzed Qualifiers

Mercury mg/kg <0.010 0.035 12/17/19 10:10

LABORATORY CONTROL SAMPLE: 1994299

Spike LCS LCS % Rec
Parameter Units Conc. Result % Rec Limits Qualifiers

Mercury mg/kg 0.83 0.89 107 85-115

MATRIX SPIKE & MATRIX SPIKE DUPLICATE: 1994300 1994301

MS MSD 40200810001 Spike Spike MS MSD MS MSD % Rec Max % Rec RPD Parameter Units Result Conc. Conc. Result Result % Rec RPD Limits Qual Mercury mg/kg < 0.010 0.89 0.88 0.96 0.99 108 112 85-115 3 20

Results presented on this page are in the units indicated by the "Units" column except where an alternate unit is presented to the right of the result.

#### **REPORT OF LABORATORY ANALYSIS**

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**QUALITY CONTROL DATA** 

Project: DEC 2019 Hg STACK TEST

Pace Project No.: 40200724

QC Batch: 343896 Analysis Method: ASTM D2974-87

QC Batch Method: ASTM D2974-87 Analysis Description: Dry Weight/Percent Moisture

Associated Lab Samples: 40200724001, 40200724002, 40200724003

SAMPLE DUPLICATE: 1996383

Date: 12/20/2019 08:58 AM

		40200908006	Dup		Max	
Parameter	Units	Result	Result	RPD	RPD	Qualifiers
Percent Moisture	%	9.7	9.4	3	10	

Results presented on this page are in the units indicated by the "Units" column except where an alternate unit is presented to the right of the result.

#### **REPORT OF LABORATORY ANALYSIS**

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#### **QUALITY CONTROL DATA**

Project: DEC 2019 Hg STACK TEST

Pace Project No.: 40200724

QC Batch: 343592 Analysis Method: EPA 160.4

QC Batch Method: EPA 160.4 Analysis Description: 160.4 Total Volatile Solids

Associated Lab Samples: 40200724001, 40200724002, 40200724003

METHOD BLANK: 1994842 Matrix: Solid

Associated Lab Samples: 40200724001, 40200724002, 40200724003

Blank Reporting

Parameter Units Result Limit Analyzed Qualifiers

Total Volatile Solids % (w/w) <30.0 30.0 12/17/19 08:42

LABORATORY CONTROL SAMPLE: 1994843

Spike LCS LCS % Rec
Parameter Units Conc. Result % Rec Limits Qualifiers

Total Volatile Solids % (w/w) 200 180 90 80-120

SAMPLE DUPLICATE: 1994844

Date: 12/20/2019 08:58 AM

40200724001 Dup Max RPD RPD Parameter Units Result Result Qualifiers Total Volatile Solids 69.1 69.5 10 % (w/w) 1

Results presented on this page are in the units indicated by the "Units" column except where an alternate unit is presented to the right of the result.

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**QUALITY CONTROL DATA** 

DEC 2019 Hg STACK TEST Project:

Pace Project No.:

40200724

QC Batch: 343593 Analysis Method:

SM 2540G

QC Batch Method: SM 2540G Analysis Description:

2540G Total Solids

Associated Lab Samples:

40200724001, 40200724002, 40200724003

METHOD BLANK: 1994845

Matrix: Solid

Associated Lab Samples:

40200724001, 40200724002, 40200724003

Blank Result Reporting

Parameter

Units

Limit

Analyzed

100

Qualifiers

Total Solids

%

<30.0

30.0 12/17/19 10:48

LABORATORY CONTROL SAMPLE:

Parameter

1994846

Spike Conc.

LCS Result

LCS % Rec % Rec Limits

Qualifiers

Total Solids

Total Solids

Units %

97.4

97.2

80-120

SAMPLE DUPLICATE: 1994847

Date: 12/20/2019 08:58 AM

Parameter

Units

%

40200741001 Result

767

Dup Result

769

RPD

Max RPD

0

Qualifiers

10

Results presented on this page are in the units indicated by the "Units" column except where an alternate unit is presented to the right of the result.

**REPORT OF LABORATORY ANALYSIS** 

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Page 11 of 16

241 Bellevue Street - Suite 9 Green Bay, WI 54302 (920)469-2436



#### **QUALIFIERS**

Project: DEC 2019 Hg STACK TEST

Pace Project No.: 40200724

#### **DEFINITIONS**

DF - Dilution Factor, if reported, represents the factor applied to the reported data due to dilution of the sample aliquot.

ND - Not Detected at or above LOD.

J - Estimated concentration at or above the LOD and below the LOQ.

LOD - Limit of Detection adjusted for dilution factor, percent moisture, initial weight and final volume.

LOQ - Limit of Quantitation adjusted for dilution factor, percent moisture, initial weight and final volume.

S - Surrogate

1,2-Diphenylhydrazine decomposes to and cannot be separated from Azobenzene using Method 8270. The result for each analyte is a combined concentration.

Consistent with EPA guidelines, unrounded data are displayed and have been used to calculate % recovery and RPD values.

LCS(D) - Laboratory Control Sample (Duplicate)

MS(D) - Matrix Spike (Duplicate)

DUP - Sample Duplicate

RPD - Relative Percent Difference

NC - Not Calculable.

SG - Silica Gel - Clean-Up

U - Indicates the compound was analyzed for, but not detected at or above the adjusted LOD.

N-Nitrosodiphenylamine decomposes and cannot be separated from Diphenylamine using Method 8270. The result reported for each analyte is a combined concentration.

Pace Analytical is TNI accredited. Contact your Pace PM for the current list of accredited analytes.

TNI - The NELAC Institute.

#### ANALYTE QUALIFIERS

Date: 12/20/2019 08:58 AM

1q Analyte was detected in the associated method blank at a concentration of -0.012 mg/kg.

C4 Sample container did not meet EPA or method requirements.

#### **REPORT OF LABORATORY ANALYSIS**

(920)469-2436



#### **QUALITY CONTROL DATA CROSS REFERENCE TABLE**

Project: DEC 2019 Hg STACK TEST

Pace Project No.: 40200724

Date: 12/20/2019 08:58 AM

Lab ID	Sample ID	QC Batch Method	QC Batch	Analytical Method	Analytical Batch
40200724001	RUN 1	EPA 7471	343458	EPA 7471	343536
40200724002	RUN 2	EPA 7471	343458	EPA 7471	343536
40200724003	RUN 3	EPA 7471	343458	EPA 7471	343536
40200724001	RUN 1	ASTM D2974-87	343896		
40200724002	RUN 2	ASTM D2974-87	343896		
40200724003	RUN 3	ASTM D2974-87	343896		
40200724001	RUN 1	EPA 160.4	343592		
40200724002	RUN 2	EPA 160.4	343592		
40200724003	RUN 3	EPA 160.4	343592		
40200724001	RUN 1	SM 2540G	343593		
40200724002	RUN 2	SM 2540G	343593		
40200724003	RUN 3	SM 2540G	343593		

#### **REPORT OF LABORATORY ANALYSIS**

special pricing and release of liability  C019a(27Jun2006)		Email #2: TYKKNZEYNEWWWARV, US Reling	it Prelin	(Rush I A I subject to approval/surcharge)  Date Needed:	o l						003 Rwn 3	, 2	ెప	DATE	EPA Level IV   NOT needed on   0 = 01	MS/MSD On your sample B = Blota	PO#: Regulatory Program:	Sampled By (Sign):	Sampled By (Print): SONNY X10NO	WI	Project Name: Dec 2019 Ha Stock Tex	Project Number:	Phone: 920-438-1045	Project Contact: TWINC MUSS	•	(Please Print Clearly) Company Name: ストからり	
Received By:	Ra	Date/Time:	13/14 8:00 WAY	Date/Time;	Date/Time: 12-12-19 Receiv						350° SI		1000   SI     X   X   X	Me To	e water nailyse	Matrix Codes  W= Water DW = Drinking Water  S Requ	747 611d	i I	PRESERVATION Pick A A A A	(YESMO) VIN N N N	H=Sodium Bisulfate Solution I=Sodium Thiosulfate J=Other	804 	CHAIN OF CUSTODY	HERE, DOCUMENTAL COLUMN	Face Analytical*	<b>-</b>	
Date/Time: Present / not Present Intact / Not Intact Version 8.0 08/14/06 OR/IGINAL		7		C Marces	Date/Time:					2	)			COMMENTS (Lab Use Only)	1 AR COMMENTS	Giveen 1	Invoice To Address: 2231 N. QUINCY	941303	•	Green Bay W 34302	Mail To Address: 2231 N. QUINCH	Mail To Company: GBMSO	Mail To Contact: TWIRE MAS	Quote#:	40200724 gge 14	IPPER MIDWEST REGION Page 1 of 1 6 11 6 12-607-1700 WI: 920-469-2436	)

F-GB-C-046-Rev.02 (29Mar2018) Sample Preservation Receipt Form

Page 1 of 2

Pace Analytical Services, LL 1241 Bellevue Street, Suite Green Bay, WI 5430

Client Name: GBMSD

Sample Preservation Receipt Form

Project #

40200724

## Pace Analytical 1241 Bellevue Street, Green Bay, WI 54302

Document Name:
Sample Condition Upon Receipt (SCUR)
Document No.:
F-GB-C-031-Rev.07

Document Revised: 25Apr2018

Issuing Authority: Pace Green Bay Quality Office

#### Sample Condition Upon Receipt Form (SCUR)

ourier: ☐ CS Logistics ☐ Fed Ex ☐ Speed ☐ Client ☐ Pace Other:	dee □ UPS □ Waltco	WO#:40200724
ustody Seal on Cooler/Box Present:  yes ustody Seal on Samples Present:  yes lacking Material:  Bubble Wrap Bulbermometer Used  SR - WA Cooler Temperature Uncorr: ROTICorr:	no Seals intact:  yes no bble Bags None Other  Type of Ice:  Blue Dry None	e 🎏 Samples on ice, cooling process has begun
Temp Blank Present:  yes  footoo Temp should be above freezing to 6°C. Siota Samples may be received at ≤ 0°C.	Biological Tissue is Froze	n:  yes no Person examining contents:  Date:
Chain of Custody Present:	ØYes □No □N/A 1. CC	12-6
Chain of Custody Filled Out:	ØYes □No □N/A 2.	
Chain of Custody Relinquished:	Øyes □No □N/A 3.	
Sampler Name & Signature on COC:	ØYes □No □N/A 4.	
Samples Arrived within Hold Time: - VOA Samples frozen upon receipt	✓Yes □No 5. □Yes □No Date/Time:	
Short Hold Time Analysis (<72hr):	□Yes □No 6.	
Rush Turn Around Time Requested:	□Yes □7No 7.	
Sufficient Volume:	SD: □Yes <b>∕</b> ENO □N/A	
Correct Containers Used:	Øyes □No 9.	
-Pace Containers Used:	□Yes □N/A □N/A	
-Pace IR Containers Used:	□Yes □No □N/A	
Containers Intact:	ZYes □No 10.	
Filtered volume received for Dissolved tests	□Yes □No □N/A 11.	
Sample Labels match COC:	Øyes_□No □N/A 12.	
-Includes date/time/ID/Analysis Matrix:	<b>D</b>	
Trip Blank Present:	□Yes □No ÞN/A 13.	
Trip Blank Custody Seals Present	□Yes □No □N/A	
Pace Trip Blank Lot # (if purchased): Client Notification/ Resolution: Person Contacted: Comments/ Resolution:	Date/Time:	If checked, see attached form for additional comments
		<u> </u>
		1, 1/2/14"

# APPENDIX F CALIBRATION DATA

Dry Gas Meter Calibration Data

Dry Gas	s Meter
Console ID:	C-10
Serial Number:	

Referenc	e Meter
Meter ID:	M5RFM1
Calibration Factor, Y <sub>w</sub> :	1.0006

Date:	01/04/19		Performed By:	LS
Barometric Pressure, P		28.67	Reviewed By:	

			Data					
				Tempe	Time			
		Reference	Dry Gas	Reference	e Dry Gas Meter			Elapsed
Vacuum	ΔН	Meter Volume	Meter Volume	Meter	init.	final	avg.	θ
(in. Hg)	(in. H <sub>2</sub> O)	$V_{w}(ft^{3})$	$V_{m}$ (ft <sup>3</sup> )	$t_{ m w}$	ti	$\mathbf{t}_{\mathrm{f}}$	t <sub>m</sub>	(min.)
5.0	0.50	5.103	5.044	63	57.0	58.0	57.5	13.00
5.0	1.00	5.042	5.044	64	59.0	61.0	60.0	9.10
5.0	2.00	5.035	5.065	64	61.0	63.0	62.0	6.25
5.0	3.00	6.029	6.122	65	62.0	64.0	63.0	6.10
5.0	4.00	5.175	5.254	65	64.0	65.0	64.5	4.50

		Calculat	ions				
ΔH	$\mathbf{Y_m}$	Vari	$\Delta H_{@}$	Variation			
(inches H <sub>2</sub> O)	(dim	ensionless)		(inches H <sub>2</sub> O)	(dimensionless)		
0.50	1.000	0.015	PASS	1.894	0.069	PASS	
1.00	0.990	0.005	PASS	1.900	0.074	PASS	
2.00	0.986	0.001	PASS	1.790	-0.035	PASS	
3.00	0.974	-0.011	PASS	1.787	-0.038	PASS	
4.00	0.975	-0.010	PASS	1.755	-0.070	PASS	
Averages:	0.985	PA	SS	1.825	PA	SS	

#### Where:

 $Y_m$  is the ratio of the reading of the reference meter to that of the dry gas meter (DGM); variance limit:  $\pm 0.02$ .

$$Y_{m} = \frac{Y_{w} V_{w} P_{b} (t_{m} + 460)}{V_{m} (P_{b} + \varnothing H/13.6) (t_{w} + 460)}$$

 $\Delta H_{@}$  is the orifice pressure differential (inches  $H_2O$ ) that corresponds to 0.75 cfm of air at 68 °F and 29.92 inches of mercury; variance limit:  $\pm 0.20$ .

$$\Delta \mathbf{H}_{@} = \frac{0.0317 \, \mathcal{Z} \mathbf{H} \, ((\mathbf{t}_{w} + 460))^{2}}{P_{b} \, (\mathbf{t}_{m} + 460) \, (\mathbf{Y}_{w} \, \mathbf{V}_{w})^{2}}$$

#### EMC Approved Alternative Method (EMC ALT-009) Alternative Method 5 Post-test Calibration

Console ID: C-10 DGM Y<sub>m</sub>: 0.985 Source: S08 Method: 29

Test Date	12/12/19	12/12/19	12/12/19	
Run #	1	2	3	
$\mathbf{Y}_{\mathbf{q}\mathbf{a}}$	0.980	0.997	0.968	dry gas meter calibration check value, dimensionless.
Test time	180	180	180	total run time, min.
Vm	114.39	111.513	116.475	total sample volume measured by dry gas meter, dcf.
Tm	541	545	544	absolute average dry gas meter temp., BR.
Pb	29.70	29.70	29.70	barometric pressure, in. Hg.
K	0.0319	0.0319	0.0319	(29.92/528)(0.75)2 (in. Hg/B/R) cfm2.
$\Delta H_{avg}$	1.27	1.24	1.27	average orifice meter differential, in. H20.
$\Delta H_{@}$	1.825	1.825	1.825	orifice meter calibration coefficient, in. H2O.
$\mathbf{M}_{ ext{d-stack gas}}$	30.06	30.05	29.99	dry molecular weight of stack gas, lb/lb-mole.
$\mathbf{M_{d-air}}$	29	29	29	dry molecular weight of air, lb/lb-mole.
$Hg_{SG}$	13.6	13.6	13.6	specific gravity of mercury.
% diff. from $Y_{\mathrm{m}}$	0.5%	-1.2%	1.7%	

<sup>\*</sup>Post-test DGM calibration check value ( $Y_{qa}$ ) must be within  $\pm 5\%$  of the specific DGM's established  $Y_m$ 



Date: 8/15/2019

DGM Model: T-110

Customer: Advanced Industrial Resources

DGM S/N: 27979

Reference Prover: Cert.# A-610 Tape # 26727

Pb:

29.89 in Ha

S-1-1-1	X 849 X		*** * * *					
Approx Flow Fato (clm)		DGM Valume (fr)	E-110	Senturo Bigni Senturo	Time (min) 0	Flow Pate (dim)	Meter Coefficient Y <sub>o</sub>	Average Meter Coefficient
0.40	2.000	2.020	76.2	76.2	5.148	0.382	0.990	
0.40	2.000	2.019	76.1	76.1	5.117	0.384	0.991	
0.40	2.000	2.009	76.2	76.2	5.122	0.384	0.996	0.992
0.60	2.000	2.018	76.5	76.5	3.320	0.592	0.991	
0.60	2.000	2.017	75.9	75.9	3.318	0.593	0.992	
0.60	2.000	2.017	75.9	75.9	3.308	0.595	0.992	0.991
0.80	2.000	2.017	75.9	75.9	2.438	0.807	0.992	
0.80	2.000	2.017	76.2	76.2	2.432	0.809	0.992	
0.80	2.000	2.023	75.9	75.9	2.428	0.810	0.989	0.991
1.00	2.000	2.022	76.3	76.3	1.943	1.012	0.989	
1.00	2.000	2.017	75.6	75.6	1.947	1.011	0.992	
1.00	2.000	2.016	76.2	76.2	1.942	1.013	0.992	0.991
1.20	2.000	2.007	75.5	75.5	1.622	1.214	0.997	
1.20	2.000	2.016	75.5	75.5	1.623	1.213	0.992	
1.20	2.000	2.017	75.5	75.5	1.623	1.213	0.992	0.993

AVERAGE Y<sub>ds</sub>

$$Y_{ds} = \frac{V_w(t_{ds} + t_{std})}{V_{ds}(t_w + t_{std})} * \frac{P_{bar}}{\left(P_{bar} + P_m/13.6\right)} \qquad Q = 17.64 \frac{P_{bar}}{\left(t_w + t_{std}\right)} \frac{V_w}{\Phi}$$

$$Q = 17.64 \frac{P_{bar}}{(t_w + t_{std})} \frac{V_w}{\Phi}$$

Dry gas meter Serial Number 27979 was calibrated in accordance with the Code of Federal Regulations, Title 40, Part 60, Appendix A, Method 5 Section 16.1.1

Signature

919-956-9688 FAX: 919-682-0333



### Quality Source Sampling Systems & Accessories

Date: 8/27/2019

DGM Model: T-110

Customer: Advanced Industrial Resources

DGM S/N: 356333

Reference Prover: Cert.# A-610 Tape # 26727

Pb:

29.86 in Hg

				*************************		***************************************		
Approx Flow Rate (crim) Q			pantri Pa	C G IA	Time (hard (h	al de la companya de	Meter Coefficient	Average Meter Coefficient
0.40	2.000	1.998	77.9	75.8	5.092	0.385	0.997	
0.40	2.000	1.997	77.4	75.8	5.088	0.385	0.999	
0.40	2.000	1.998	77.4	75.7	5.097	0.385	0.998	0.998
0.60	2.000	2.004	75.8	75.8	3.290	0.598	0.998	
0.60	2.000	2.003	75.8	75.8	3.288	0.598	0.999	
0.60	2.000	2.003	75.8	75.8	3.285	0.599	0.999	0.998
0.80	2.000	2.006	75.8	75.8	2.453	0.801	0.997	
0.80	2.000	2.007	75.8	75.8	2.442	0.805	0.997	
0.80	2.000	2.001	75.5	75.5	2.440	0.806	1.000	0.998
1.00	2.000	2.001	75.9	75.9	1.918	1.025	1.000	
1.00	2.000	2.006	75.9	75.9	1.925	1.021	0.997	
1.00	2.000	2.010	75.9	75.9	1.928	1.019	0.995	0.997
1.20	2.000	2.007	75.9	75.9	1.595	1.232	0.997	
1.20	2.000	2.006	75.9	75.9	1.597	1.231	0.997	
1.20	2.000	2.006	75.9	75.9	1.588	1.238	0.997	0.997

AVERAGE Y<sub>ds</sub>

$$Y_{ds} = \frac{V_w(t_{ds} + t_{std})}{V_{ds}(t_w + t_{std})} * \frac{P_{bar}}{\left(P_{bar} + P_m/13.6\right)} \qquad Q = 17.64 \frac{P_{bar}}{\left(t_w + t_{std}\right)} \frac{V_w}{\Phi}$$

$$Q = 17.64 \frac{P_{bar}}{(t_w + t_{std})} \frac{V_W}{\Phi}$$

Dry gas meter Serial Number 356333 was calibrated in accordance with the Code of Federal Regulations, Title 40, Part 60, Appendix A, Method 5 Section 16.1.1

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919-956-9688 FAX: 919-682-0333

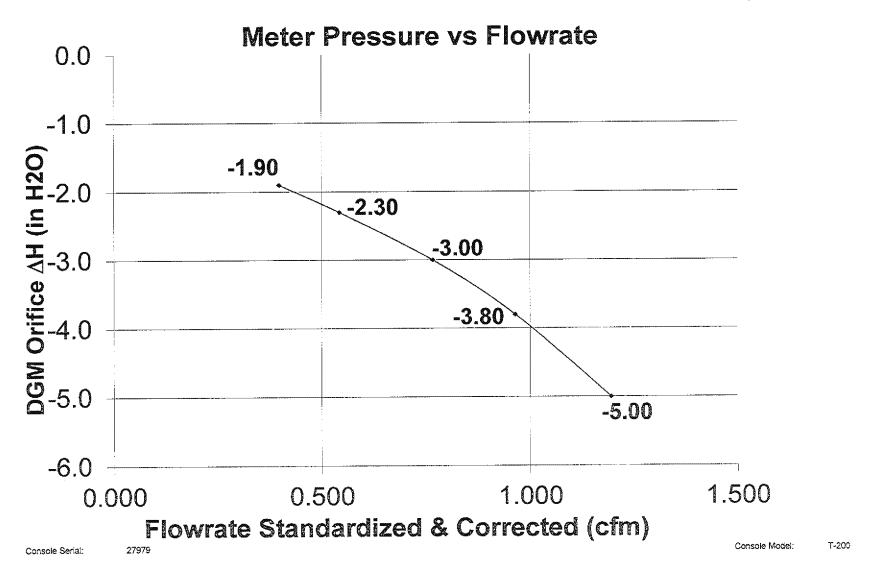
Calibration Technician: ΕW 10-10-2017 Calibration Date: **Meter Gamma vs Flowrate** 1.025 1.020 1.015 1.010 3.005 3.000 3.000 3.000 3.000 3.000 1.0054 1.0038 1.0013 -
Gamma Y -----Max Allow Y 0.9983 - Min Allow Y 0.9938 0.985 0.980 0.975 50 0.500 0.750 1.000 27979 Flowrate Standardized & Corrected (cfm) 0.250 1.250 Console Serial: Console Model: T-200

Calibration Date:

10-10-2017

Calibration Technician:

FW



#### Thermocouple Calibration Data

 Thermometer ID:
 RT-01; RT-03
 Date:
 12/20/19

 Bias:
 0
 Performed By:
 JG

Apparatus ID	Apparatus Description	Reference Temperature Reading			cated erature	Relative Variation
		۰F	°R	o <b>k</b>	°R	%
P4-01	Stack Temp.	32	492	33	493	0.2
P4-01	Stack Temp.	210	670	211	671	0.1
B-16	Filter Temp.	32	492	32	492	0.0
B-16	Filter Temp.	210	670	210	670	0.0
B-16	Exit Imp. Temp.	32	492	32	492	0.0
B-16	Exit Imp. Temp.	210	670	211	671	0.1
C-010	Meter In Temp.	32	492	33	493	0.2
C-010	Meter In Temp.	210	670	212	672	0.3
C-010	Meter Out Temp.	32	492	32	492	0.0
C-010	Meter Out Temp.	210	670	211	671	0.1
B-16	Filter Exit Temp.	32	492	33	493	0.2
B-16	Filter Exit Temp.	210	670	210	670	0.0
P4-01	Probe Temp.	32	492	33	493	0.2
P4-01	Probe Temp.	210	670	210	670	0.0

#### **Thermocouple Calibration Procedure**

#### A. References

- 1. Mercury-in-glass refernce thermometer, calibrated against thermometric fixed points.
- 2. Thermometric fixed points, including ice bath and boiling water (corrected for barometric pressure)

#### B. Measurement

1. Compare field temperature sensors against the reference thermometer. Agreement must be within  $\pm 1.5\%$  of the absolute reference temperature.

### VERIFICATION OF CONSTRUCTION SPECIFICATIONS FOR THE TYPE-S PITOT TUBE

Thomas R. Clark, Wade Mason, Paul Reinermann III PEDCo Environmental, Inc., Cincinnati, Ohio

Revisions to EPA Reference Method 2 - Determination of Stack Gas Velocity and Volumetric Flow Rate (Type-S Pitot Tube) - promulgated August 18, 1977, exempted certain pitot tubes from calibration and included appropriate construction criteria and application guidelines.

Figure 1 summarizes procedures for determining the calibration coefficients of Type-S pitot tubes. A pitot tube may be calibrated using procedures outlined in Method 2 or assigned a baseline coefficient ( $C_p$ ) of 0.84 if it meets the following criteria:

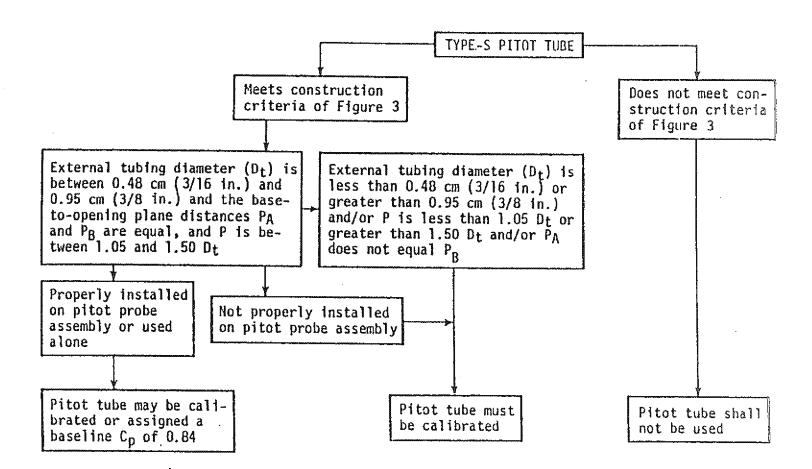
Pitot tube meets the construction criteria of Figures 2 and 3

The external tubing diameter  $(D_t)$  is between 0.48 and 0.95 cm (3/16 and 3/8 in.)

The base-to-opening plane distances (P  $_{\rm A}$  and P  $_{\rm B})$  are equal and range between 1.05 and 1.50 D  $_{\rm t}$ 

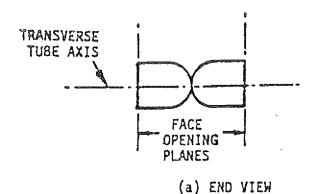
The pitot tube is used separately, or in a pitot-probe assembly, mounted in accordance with the specifications in Figures 4 and 5

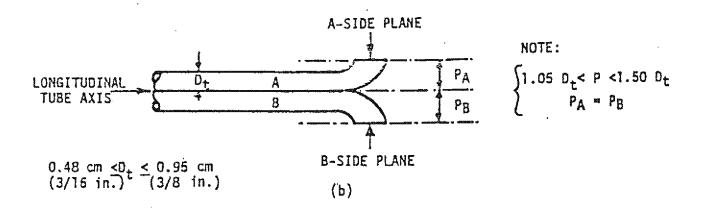
Pitot tubes that meet the construction criteria of Figures 2 and 3, but do not meet the specified limits for  $D_{t}$ ,  $P_{A}$ , and  $P_{B}$  may be used, but must be calibrated.



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Figure 1. Procedures for determining the calibration coefficients of Type-S pitot tubes.





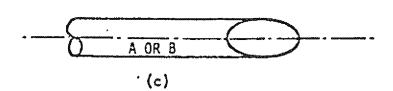


Figure 2. Properly constructed Type-S pitot tube, shown in:
(a) end view; face opening planes perpendicular to transverse axis; (b) top view; face opening plans parallel to longitudinal axis; (c) side view; both legs of equal length and centerlines coincident, when viewed from both sides. Baseline coefficient values of 0.84 may be assigned to pitot tubes constructed this way.

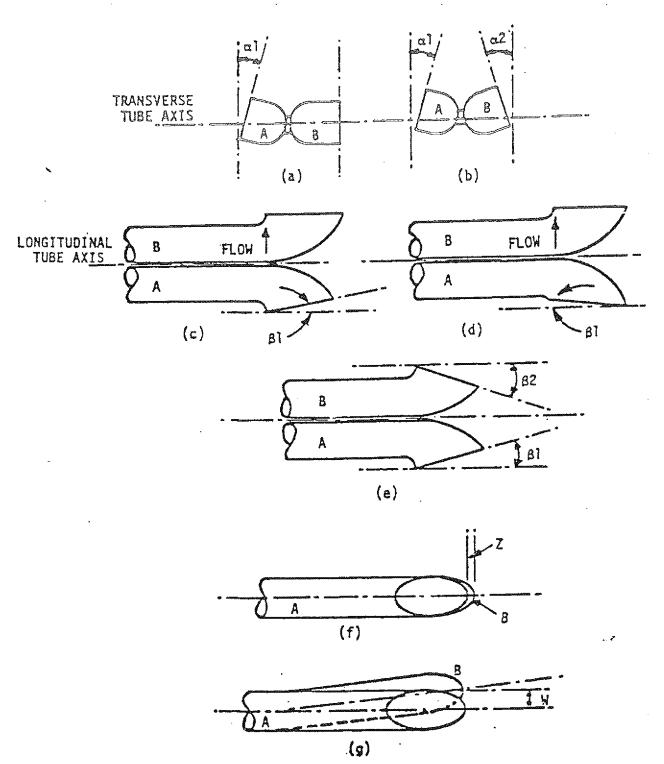
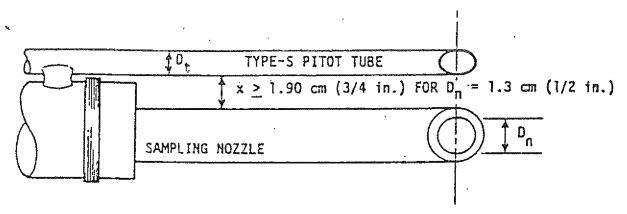
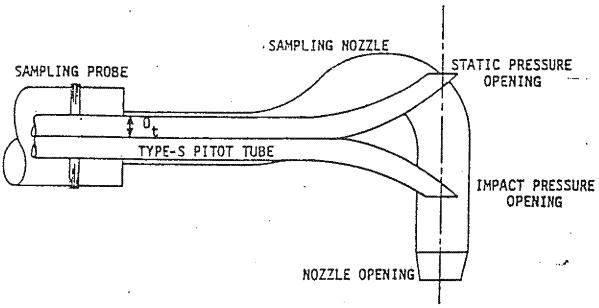


Figure 3. Types of face-opening misalignment that can result from field use or improper construction of Type S pitot tubes. These will not affect Cp as long as all and a2 <10°,  $\beta$ 2 <5°, z <0.32 cm (1/8 in.) and w <0.08 cm (1/32 in.).

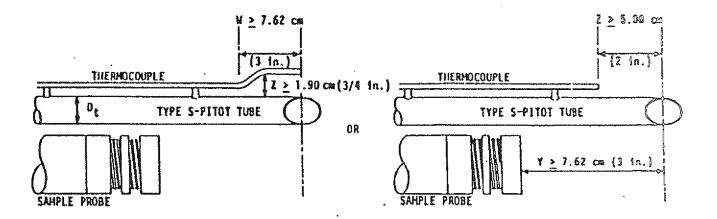


A. BOTTOM VIEW: SHOWING MINIMUM PITOT-NOZZLE SEPARATION.



B. SIDE VIEW: TO PREVENT PITOT TUBE FROM INTERFERING WITH GAS FLOW STREAMLINES APPROACHING THE NOZZLE, THE IMPACT PRESSURE OPENING PLANE OF THE PITOT TUBE SHALL BE EVEN WITH OR ABOVE THE NOZZLE ENTRY PLANE.

Figure 4. Required pitot tube - sampling nozzle configuration to prevent aerodynamic interference; buttonhook - type nozzle; centers of nozzle and pitot opening aligned; D<sub>t</sub> between 0.48 and 0.95 cm (3/16 and 3/8 in.).



O

Figure 5. Required thermocouple and probe placement to prevent interference; D<sub>t</sub> between 0.48 and 0.95 cm (3/16 and 3/8 in.).

ED\_012958\_00013359-00095

The EPA has not specified a measurement technique to verify proper construction. The following procedures provide a quick and accurate method of checking construction specifications for Type-S pitot tubes. The apparatus is inexpensive and available in most hardware stores. The method can be used in the laboratory by testers and easily adapted to field use by agency personnel while witnessing tests or performing quality assurance checks.

- 1. Obtain a section of angle aluminum approximately 20 cm (8 in.) by 1.3 x 2.5 cm (0.5 x 1.0 in.). Mount a bull's-eye level (with ±1 degree accuracy) to the angle aluminum, as shown in Figure 6. After mounting the buil's-eye level to the angle aluminum, level the angle aluminum and place the degree-indicating level in the parallel and perpendicular positions. The indicating level should not read more than 1 degree in either position.
- 2. Place the pitot tube in the angle aluminum as shown in Figure 6, and level the pitot tube as indicated by the bull's-eye level. A vise may be used to hold the angle aluminum and pitot tube in the laboratory and a C-clamp in the field.

  Note: A permanently mounted pitot tube and probe assembly may require a shorter section of angle aluminum to allow proper mounting on the assembly.
- Place a degree-indicating level in the various positions, as illustrated in Figures 7 and 8.
  - Measure distances P<sub>A</sub> and P<sub>B</sub> with a micrometer.

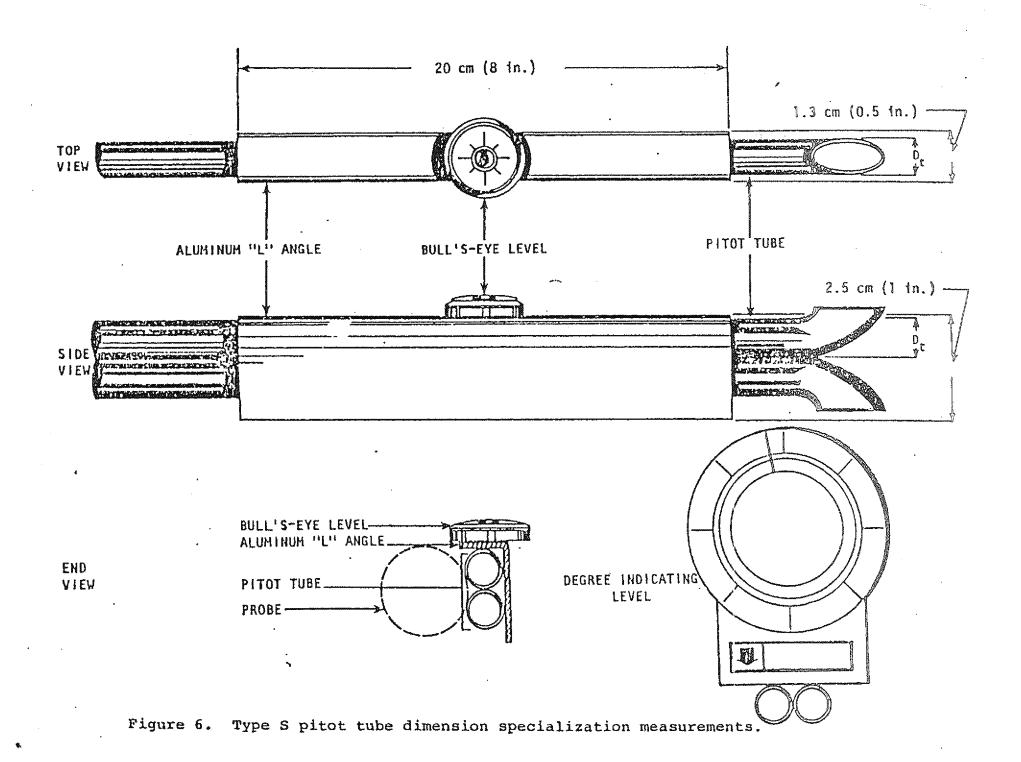
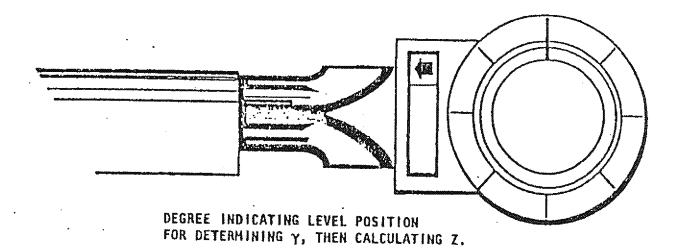


Figure 7 Position of dimension measurement.



DEGREE INDICATING LEVEL POSITION FOR DETERMINING  $\Theta$ , THEN CALCULATE W.

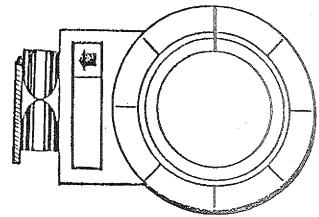


Figure 8. Position of dimension measurement.

- 5. Measure the external tube diameter ( $D_t$ ). Record all data on a data sheet such as Figure 9.
- 6. Calculate dimensions w and z using the following equations:

$$w = A \sin \theta$$

Equation 1

 $r = A \sin \gamma$ 

Equation 2

where,

w = alignment dimension, cm (in.)

z = alignment dimension, cm (in.)

 $A = distance between tips, (P_A + P_B), cm (in.)$ 

 $\Theta$  = angle in degrees

 $\gamma$  = angle in degrees.

Note: Pitot tubes with bent or damaged tubing may be difficult to check using this procedure.

If the Type-S pitot tube meets the face alignment criteria, an identification number should be assigned and permanently marked or engraved on the body of the tube.

#### References

1. Federal Register, Vol. 42. No. 160, August 18, 1977.

## Advanced Industrial Resources, Inc. Type-S Pitot Tube Assembly Inspection Data Sheet

Date:	12/20/2019							
Pitot Tube Assembly:	P4-01	Caliper ID: CL-04						
Performed by:								
Pitot tube assembly level?	X yes	no						
Pitot tube openings damaged?	yes (expla	nin below) X no						
<sub>1</sub> = o(<10°)	<sub>1</sub> =1	°(<5°)						
<sub>2</sub> = o(<10°)	2= 1							
= =	o A=	in.						
$z = A \sin \gamma = \underline{0.0000}$	in. <1/8 in. (0	0.125 in.)						
$\mathbf{w} = \mathbf{A} \sin \theta = \underline{0.0000}$	in. <1/32 in.	(0.03125 in.)						
$P_{A} = 0.450$ in.	$P_{B} = 0.450$	in.						
$D_t = _{\underline{\hspace{1cm}} 0.35} in.$	$\mathbf{P} / \mathbf{D_t} = \underbrace{1.28571}_{\mathbf{P_a} = \mathbf{P_b} = }$	(1.05 = and </= 1.50)</td						
X = 0.97 (>0.75 in.) Y = 3.7 (>3.0 in.) Z = 2.3 (>0.75 in.)	(Dist. from nozzle u	een pitot and nozzle) union to pitot tube openings) ot and stack thermocouple)						
Does the pitot tube assembly meet the Method 2 requiremnets? X yes no (explain below)								
•	pitot tube assembly be							

Nozzle Calibration Data

Client:	Green	Day	MSD	Date: _	12-12-14
Location:	Green	Bey		Performed By:	JC.
			•	Caliper ID:	62-04

Source	Nozzle	Nozzle	М	Average			
	TD	Description	1	(inches)	3	(inches)	
Incinenter 1	610-1-2	blass	0.200	0.200	0.200	6.200	
	17.0						
	- Transcrossor that how the single-function of the signs of the sign of						
	e de la companya de l	<b>V</b>					
	,		ļ				

Test Team Leader Review:

Data Entry Review:

#### Analyzer Pretest Data Worksheet

Operator Name:	Greg Essig	Source ID:	Stack S08
Facility Name, Location:	Green Bay MSD Green Bay, WI	Date:	12/12/19
Analyte 1:	Oxygen O2	EPA Method:	3A
•	Carbon Dioxide CO2	EPA Method:	3A

#### Calibration Gas Serial Numbers & Concentrations

Gas (Zero, Low, Mid and High)	Analyzer I.D.	Concentration (% or ppm)	Cylinder ID #	Expiration Date	Manufacturer
Zero (N2 or Air)	NA	0.00	0	1/0/1900	0
O2/ CO2 (Mid)	10	11.3/8.584	EB0094466	9/23/2027	Airgas
O2/ CO2 (High)	10	19.77/18.05	CC716961	9/24/2027	Airgas

#### **Stratification Worksheet**

Stack Dimensio	on & 12-pt Traverse	Point Location	Stack Dimensi	on & 3-pt Traverse	Point Location			
Enter the stack d	iameter here $(D_s) \rightarrow$	23.5	Stack Diameter $(D_s) \rightarrow 23.5$					
Traverse Point No.	% of D <sub>s</sub>	Actual Inches	Traverse Point No.	% of D <sub>s</sub>	Actual Inches			
1	2.1%	0.49	1	16.7%	3.92			
2	6.7%	1.57	2	50.0%	11.75			
3	11.8%	2.77	3	83.3%	19.58			
4	17.7%	4.16						
5	25.0%	5.88						
6	35.6%	8.37						
7	64.4%	15.13	Stack was tra	versed during	testing using			
8	75.0%	17.63	Juck was na	_	, testing using			
9	82.3%	19.34	12 points					
10	88.2%	20.73						
11	93.3%	21.93	1					
12	97.9%	23.01						





#### CERTIFICATE OF ANALYSIS

**Grade of Product: EPA Protocol** 

Part Number:

E03NI62E15A1071

CC716961

Cylinder Number: Laboratory:

PGVP Number: Gas Code:

124 - Durham (SAP) - NC

B22019

CO2,O2,BALN

Reference Number:

122-401601514-1

Cylinder Volume:

157.9 CF

Cylinder Pressure:

2015 PSIG

Valve Outlet:

590

Certification Date:

Sep 24, 2019

Expiration Date: Sep 24, 2027

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig. i.e. 0.7 megapascals,

			A DATA T TOTAL			
Component Requested Concentration		ANALYTICAL RESULTS Actual Protocol Concentration Method		Total Relative Uncertainty	Assay Dates	
CARBON	DIOXIDE	18.00 %	18.05 %	G1	+/- 0.6% NIST Traceabl	e 09/24/2019
OXYGEN		20,00 %	19.77 %	G1	+/- 0.5% NIST Traceabl	e 09/24/2019
NITROGE	N .	Balance				
Туре	Lot ID	Cylinder No	CALIBRATION Concentration	N STANDARD	S Uncertainty	Expiration Date
NTRM	12061508	CC354696	19,87 % CARBON D	IOXIDE/NITROGEN	+/- 0,6%	Jan 11, 2024
NTRM	08010202	1D003076	23.20 % OXYGEN/N	IITROGEN	+/- 0.4%	Jun 01, 2024
Instrume	nt/Make/Mod	el	ANALYTICAL Analytical Princip	-	r Last Multipoint C	alibration
	510 CO2 2L6Y A510 O2 41499		Nondispersive Infrare		Sep 05, 2019 Sep 05, 2019	

Triad Data Available Upon Request



Approved for Release

Page 1 of 122-401601514-1





#### CERTIFICATE OF ANALYSIS

#### **Grade of Product: EPA Protocol**

Part Number: Cylinder Number: E03NI80E15A0007

Laboratory:

PGVP Number:

EB0094466

Gas Code:

B22019

CO2,O2,BALN

124 - Durham (SAP) - NC

Cylinder Volume:

Reference Number: 122-401602294-1

Cylinder Pressure:

150.4 CF 2015 PSIG

Valve Outlet:

590

Certification Date:

Sep 23, 2019

Expiration Date: Sep 23, 2027

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

	ANALYTICAL RESULTS								
Component Requested Concentration		**		Total Relative Uncertainty	Assay Dates				
CARBON	RBON DIOXIDE 9,000 % 8.584 % G1		. G1	+/- 0.6% NIST Traceable	09/23/2019				
OXYGEN		11.00 %	11,30 %	11,30 % G1		09/23/2019			
NITROGE	Ν	Balance		2211442330003211334452330022104352104323124323132433	umurs (conservation) and an arrangement of the conservation of the				
CALIBRATION STANDARDS									
Туре	Lot ID	Cylinder No	Concentration		Uncertainty	Expiration Date			
NTRM	13060638	CC414571	13,359 % CARBON (	DIOXIDE/NITROGEN	+/- 0.6%	May 14, 2025			
NTRM	09060212	CC262381	9.961 % OXYGEN/N	ITROGEN	+/- 0,3%	Nov 05, 2024			
	ANALYTICAL EQUIPMENT								
	nt/Make/Mod	Total Control State Control St		Analytical Principle		lbration ·			
	\510 CO2 2L6Y		Nondispersive Infrare	d (NDIR)	Sep 05, 2019				
Horiba MF	A510 O2 41499	150042	Paramagnetic		Sep 05, 2019				

Triad Data Available Upon Request



Approved for Release

# APPENDIX G PROCESS OPERATION DATA

# GBMSD Stack Testing Results Green Bay Facility - Fluid Bed Incinerator BFP Sludge Cake Solids 12/12/2019

					Gallons/	Wet	Dry	Dry
DATE	Run	LAB NO.	SAMPLE	%TS	hr	lbs/hr	lbs/hr	ton/hr
12/12/2019	Run #1	RUN 1	RUN 1	34.9	1145.4	10446	3646	1.823
12/12/2019	Run #2	RUN 2	RUN 2	35.5	1124.3	10253.6	3640	1.820
12/12/2019	Run #3	RUN 3	RUN 3	36.2	1076.6	9818.59	3554	1.777



for All of Us®

#### TECHNICAL MEMORANDUM

TO: FILE

FROM: Jeremy Luebke

DATE: January 23, 2020

RE: Analysis of Impact of Mercury Emissions from FBI

SEH No. 153650 GODFR

The Green Bay Metropolitan Sewerage District (GBMSD) operates a fluid bed incinerator (FBI) and associated air pollution control equipment at their wastewater treatment plant located in Green Bay, Wisconsin. The purpose of this memorandum is to evaluate the potential impacts of operating the FBI without one of the emission control system, the Granular Activated Carbon (GAC) system. The GAC is designed to control mercury emissions.

The purpose of this memorandum is to document that the GBMSD demonstrates compliance with Wisconsin Administrative Code Chapter NR 445 Table A - *Emission Thresholds, Standards and Control Requirements for All Sources of Hazardous Air Contaminates*, specifically for mercury compounds, from the FBI (I08) when the GAC control device is offline.

NR 445.07 Emission thresholds, standards, control requirements and exemptions, paragraph (1)(a) states the following:

No owner or operator of a source may cause, allow or permit emissions of a hazardous air contaminant listed in Table A in such quantity or concentration or for such duration as to cause an ambient air concentration of the contaminant off the source property that exceeds the concentration in column (g) of Table A for the contaminant.

Column (g) of Table A lists the Ambient Air Standard (per time period in column h expresses as micrograms per cubic meter).

NR 445.08 describes the acceptable methods by which to demonstrate compliance with the Ambient Air Standards in Table A. NR 445.08(1) requires that the determination of compliance shall be done while the source is operating under normal permit conditions, or in the absent of a permit, the maximum theoretical emissions. The incinerator mercury emission rate was determined in a December 12, 2019 stack test. The incinerator was operating under permit compliant conditions without the GAC operating, resulting in a worst-case scenario emission rate for mercury emissions. The emission rate for mercury, averaged over all three runs is 0.000646 lb/hr.

#### Compliance Demonstration via NR 445.08(2)(a) – Thresholds for Emission Rates

The first method that can be used to demonstrate compliance, as provided in NR 445.08(2), paragraph (a) is to show that emissions from the incinerator are below Table A Thresholds for Emission Points (expressed as pounds per hour or pounds per year) in columns (c), (d), (e), or (f), depending on stack height. The incinerator stack height has a height of 120 feet above grade, requiring emissions to be

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compared to column (f) "Emissions from Stacks ≥75 ft" threshold values. If the source has emission rates less than the thresholds in Table A, column (f), it is assumed that the Ambient Air Standards in column (g) will not be exceeded.

NR 445.07 Table A, column (f) threshold values are not exceeded for inorganic mercury. In the following **Table 1 – Mercury Emission Rate Comparisons to Table A Thresholds for Emission Points**, Table A threshold values are compared to the stack test incinerator emission rate.

**Table 1 – Mercury Emission Comparison** 

	December 2019 Stack Test (lb/hr)	December 2019 Stack Test (lb/yr)	Table A Thresholds for Stacks ≥75 ft (lb/hr)	% of Table A Thresholds
Ца	0.000646	-	0.0405	1.60%
Hg	-	5.66	1,838	0.31%

Note: The annual emission rate is the hourly rate, 0.000646 lb/hr, multiplied by 8,760 hour per year.

#### Compliance Demonstration via NR 445.08(2)(b) - Ambient Air Concentrations

Secondly, NR 445.08(2) paragraph (b) provides the option to demonstrate that the ambient air concentration off the source property is less than the column (g) "Ambient Air Standards" for mercury are surpassed. This demonstration is conducted through dispersion modeling as shown below.

This dispersion modeling analysis was performed using the AMS/EPA Regulatory Model (AERMOD) (Version 18081) with the Lakes® AERMOD user interface. Five years (2011-2015) of preprocessed meteorological data, obtained from the WDNR website, were used in this analysis. The surface meteorological and upper air meteorological data were taken from the Green Bay, WI station.

The receptors used in this analysis consisted of a grid with fenceline receptors placed every 50 meters, 50-meter receptor resolution out to a distance of one kilometer, and receptors placed every 200 meters until a distance of two kilometers. Receptor points within the facility were not considered. As per WDNR policy, terrain elevations as derived from AERMAP were incorporated in the modeling analysis. Elevations were determined using USGS National Elevation Dataset (NED) files obtained from the USGS National Map Seamless Server website. USGS NED data is in conformance with the North American Datum of 1983 (NAD 83).

Previous WDNR modeling parameters for the incinerator (I08) were used for stack location, height, and diameter. However, for this modeling exercise, actual measured parameters from the December 2019 stack test were used for exhaust temperature, exit velocity, airflow and emission rate. Parameters can be found below in **Table 2**.

Table 2 - Modeling Input Parameters

		х	Y	Base Elevation	Height	Diameter	Rainhat	Exhaust Temp	Exit Velocity	Air Flow	Mercury
Stack ID	Description	meters	meters	meters	feet	feet	Y/N	F	m/s	acfm	lb/hr
108	Fluid Bed Incinerator	420555	4931795.4	179.0	120	2.0	N	113.3	15.63	9,267	0.000646

Ambient air standards are not surpassed in this dispersion modeling demonstration. Modeling results are shown below in **Table 3**.

Table 3 - Modeling Results Compared to Table A Ambient Air Standards

	Averaging Period	Statistic / Metric	Modeled Concentration (μg/m³)	NR 445 Ambient Air Standards (µg/m³)	% of NR 445
Hg	24-hr	1st Highest	0.00187	0.6	0.3%
	Annual	1st Highest	0.00004	0.3	0.01%

#### Conclusions

The District can demonstrate compliance with NR 445.07(1) requirements. Uncontrolled mercury emissions from the incinerator do not surpass Table A, column (f) Thresholds for Emission Points or column (g) Ambient Air Standards.

#### JTL/pas

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